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초광대역 테라헤르츠 전자기파를 이용한 퓨리에 광학 현상 및 응용 연구

Fourier optical phenomena and applications using ultra broadband terahertz waves

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A thesis submitted to the faculty of KAIST in partial fulfillment of the requirements for the degree of Doctor of Philosophy in the Department of Physics . The study was conducted in accordance with Code of Research Ethics¹.

> 2013. 5. 23. Approved by Professor Ahn, Jaewook [Advisor]

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ABSTRACT

Pulsed terahertz (THz) waves which are generated from femtosecond laser pulses have ultra-broad bandwidth compared to other frequency electromagnetic waves. In addition, phase measurement of pulsed THz waves is very convenient because we can directly measure the field of them. In this dissertation, we study Fourier optical phenomena and their applications with these ultra broadband pulsed THz waves.

Diffraction pattern can be achieved by spectral analysis of ultra broadband THz waves instead of scan detection. With this principle, we demonstrate three different single-pixel diffraction imaging systems which need only one dimensional data acquisition processes for two dimensional imaging. In the first experiment, we set a coherent optical computer and show that complex 2D images are reconstructed with only 30 waveform measurements by rotating a hole mask placed in the spatial frequency domain. In the second, we also demonstrate one waveform diffraction imaging with the time separating hole mask in the coherent optical computer. In the last experiment, we use a wedge prism, or a slanted phase retarder, instead of the coherent optical computer and achieve much higher signal-to-noise-rate imaging.

Polarization of ultra broadband THz waves is not easily represented by polarization theories of monochromatic waves. To show this, we shape unconventional polarization states of few-cycle THz pulse by illuminating spatiotemporal controlled ultrafast laser pulses on a circularly metal-patterned InAs thin film surface. For this polarization shaping, a set of wedges having various directions and thicknesses are arranged to achieve proper spatiotemporal controlling of ultrafast laser pulses. By them, we generate THz waves of various uncommon polarization states, such as polarization alternation between right and left circular polarization states. We also define a time domain representation of polarization to analyze these types of polarization.

We also study sub-wavelength diffraction and, especially, focus to study of phase shift anomalies caused by sub-wavelength diffraction. From scalar diffraction theories, it is generally known that $-\pi/2$ phase shift, or Gouy phase shift, happens in normal diffraction cases. By direct field measurement in THz time domain spectroscopy, we demonstrate that the phase shift can vary between 0 to $-\pi$, instead of the constant, $-\pi/2$, in sub-wavelength diffraction. Nearly $\pi/2$ phase retardation with respect to the Gouy phase shift happens in transmission through a small slit perpendicular to the electric field, while nearly $\pi/2$ phase advance happens in transmission through a small slit parallel to the electric field or a small circular hole. The physical reason of these disagreements is plasmon coupling or magnetic dipole radiation. Due to these phase shift anomalies, diffraction pattern is also modulated from the expectation of the scalar diffraction theory, and we study sub-wavelength Young's double-slit experiment to demonstrate it.

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Chapter 1. Introduction

Fourier optics is the study of wave optics with Fourier transform. The nature of light is explained by the wave equation, and several key physical quantities of light, such as time and frequency, are related by Fourier theory. Therefore, many optical phenomena are easily understood from Fourier analyses, and various optical applications like imaging processing can be derived by its mathematical power.

Although its long development history, newly developed terahertz (THz) waves can stimulate more studies in Fourier optics. Here, THz waves usually represent the electromagnetic waves whose frequency range is between 0.1 THz and 10 THz (1 THz = 10^{12} Hz). Due to inefficient generating and detecting techniques for THz waves, this electromagnetic spectrum was historically not much studied, and usually called as "THz Gap". However, over the last two decades, studying to pioneer this undeveloped spectrum has been very active, and THz technologies are more available nowadays than before. The key advantage of THz technologies for Fourier optics is that THz waves have both long-wave and short-wave properties simultaneously. Like longer electromagnetic waves, direct phase measurement is conventional in THz range, and THz waves can also have ultra-broad bandwidth, the frequency-to-bandwidth ratio of near unity, like radar pulses. On the other hand, wavelength of THz waves is short enough to follow various Fourier optical theories, such as the Fraunhofer diffraction equation, in conventional optical table size experiments. Therefore, THz waves are located at the ideal frequency band to study of Fourier optical phenomena related to broad bandwidth or phase.

In this dissertation, we study Fourier optical phenomena, such as diffraction, with ultra broadband THz waves and suggest their applications based on these novel characters of ultra broadband THz waves.

Terahertz time domain spectroscopy (THz-TDS) with ultrafast femtosecond lasers is the key technique in THz researches, and all experiments in this dissertation are based on this technique. Therefore, understanding THz-TDS is an essential prerequisite to understand this dissertation, and we review THz-TDS based on ultrafast laser system in Chapter 2. We review properties of THz waves in this system more specifically and review THz generation and detection methods. In addition, we also discuss the calculation of the refractive index with real data from THz-TDS measurment as an example in THz-TDS usage.

Imaging is one of the most important research topics in optics, and the diffraction imaging process possesses the biggest part of Fourier optical applications. In diffraction imaging, monochromatic waves are generally considered, but data accumulation process can be much simplified with ultra broadband THz waves. In Chapter 3, we demonstrate that ultra-broad bandwidth can replace radial direction data accumulation in the Fourier domain, and, as a result, single-pixel imagery is realized with THz waves. Three different experimental setups based on this scheme are presented in Chapter 3, and images are well reconstructed by these setups.

Time varying polarization states of ultra broadband waves are not considered in traditional optics, but rapid temporal change of polarization is possible with ultra broadband THz waves. In Chapter 4, we synthesize these unconventional polarization states with few-cycle THz waves. For this, a set of N femtosecond laser pulses arranged in space and time is generated from a devised diffractive optical system made of as-many glass wedges, which then illuminates a sub-wavelength metal pattern of an indium arsenide thin film and produces THz waves of tailor-made polarization states given as a superposition of N linearly-polarized THz pulses. By properly superposing temporally-shifted linear polarization components, we successfully generate THz waves of various polarization states, such as polarization rotation and alternation between circular polarization states. We also analyze these polarization states with our own representation which one not fully described by monochromatic analysis.

It is known that scalar diffraction theories can not be applied in sub-wavelength diffraction, but phase studies are not much considered since phase measurement of light is not straightforward in other frequency ranges. In Chapter 5, we investigate phase shift anomalies that are caused by wave diffraction from a slit or a circular aperture of sub-wavelength scale. Nearly $\pi/2$ -phase delay from a small perpendicular slit and $\pi/2$ -phase advance from a small parallel slit, and also from a small circular aperture, have been directly measured. These results demonstrate that the common $\pi/2$ phase advance of diffraction waves in the far-field region, known as Gouy phase shift, is not valid in sub-wavelength diffraction, and, instead of that, phase shifts can vary from 0 to π with respect to the propagating factor, e^{ikR} . Physical origin of these phase shift anomalies is plasmon coupling or magnetic dipole radiation, and theoretical predictions based on these models are in good agreement with the experimental results. Due to these phase shift anomalies, diffraction pattern is also modulated from the expectation of scalar diffraction theories, and we verify this modulation by studying sub-wavelength Young's double-slit experiment.

Chapter 2. Terahertz waves in terahertz time domain spectroscopy

2.1 Introduction

In photonics community, ultrashort or ultrafast femtosecond pulses denote electromagnetic pulses whose time durations are the order of the femtosecond (1 fs= 10^{-15} s). These pulses have a broadband optical spectrum due to the uncertainty principle, and can be created by mode-locked laser technologies such as a passive mode-locked 800 nm-centered Ti:Sapphire laser. With these laser technologies, numerous applications, such as ultrafast time-resolved spectroscopy [1, 2, 3], micro-machining [4, 5], coherent control [6, 7, 8, 9, 10], precision measurement [11, 12], and bio imaging [13, 14], are convenient nowadays.

Terahertz time domain spectroscopy (THz-TDS) is one of the important applications in these femtosecond laser technologies. In THz-TDS, one generates THz pulses and measures their fields directly in time domain with femtosecond laser pulses. Because of its convenience compare to other THz techniques, THz-TDS is placed on the center of THz applications including THz spectroscopy and THz imaging.

There are two characters which distinguish THz-TDS from other THz techniques. Firstly, generated THz waves in THz-TDS are few-cycles or sub-cycle pulses, so they have ultra-broad bandwidth. Here, we define ultra-broad bandwidth as bandwidth having the frequency-to-bandwidth ratio of near unity in this dissertation. The second one is direct phase measuring capability of THz waves. In THz-TDS, one detects the field of THz waves in time domain directly, so phase information of THz waves can be obtained by conventional Fourier transform process.

All THz researches in this dissertation are based on THz-TDS, and these researches are strongly related with the above two characters. Due to the significance of them, we review the THz-TDS technique in this chapter. After then, we briefly discuss the calculation of refractive index in transmission geometry of THz-TDS in order to demonstrate these special advantages of THz-TDS.

2.2 Terahertz spectrum

THz spectrum is placed between 0.1 THz and 10 THz. Electromagnetic waves with 1 THz, which is the center frequency of THz range, corresponds to the following physical quantities.

$$1 \text{THz} \sim 300 \mu \text{m} \sim 33 \text{cm}^{-1} \sim 1 \text{ps} \sim 4.14 \text{meV} \sim 48 \text{K}$$
 (2.1)

This frequency range was traditionally called "far-infrared" or "sub-millimeter waves" but "THz waves" or "T-ray" is more common name nowadays. This frequency range is located between the microwave and infrared bands as shown in Fig. 2.1. Historically, this frequency range was too high to be radiated with electronic technologies and too low to be generated with photonic technologies. In addition, many absorbing energy levels of the atmosphere, especially water vapor, are placed in this frequency range [15, 16], so wave transferring is even a challenge. As a result, this range has been usually called as "THz Gap". On the other hand, these waves have duality of electric waves and light, and the duality is actively used in various research fields including ones in this dissertation.



Figure 2.1: THz spectrum. THz range is located between electronics and photonics.

Although spectroscopic applications of THz waves are not much considered in this dissertation, we mention of them briefly due to their technological importance. It is known that THz range involves vibration and rotation levels of water and molecules [17, 18], these frequencies can become chemical fingerprints, so nondestructive testing or a bio application is expected. For examples, drug examinations [19, 20] or weapon inspection in airport is already available, and THz breast cancer inspection is about to be used [21].

2.3 Generation of terahertz waves in THz-TDS

We briefly introduce two types of T-ray generation methods related with this dissertation, which are photoconductive antenna and photo-Dember currents. Although optical rectification is another important THz generation method [22, 23, 24], we skip it in this dissertation.

2.3.1 Photoconductive antenna

When ultrafast femtosecond laser beams illuminate on semiconductor surfaces, photo-carriers are created. Then, these photo-carriers could flow due to drift or diffusion, and electromagnetic waves radiate by these currents.

Photoconductive antenna(PCA) uses drift currents. This device is invented by Austin, so it is sometimes called as Auston switch [25]. The principle of T-ray generation in PCA is shown in Fig. 2.2. PCA is composed of two electrodes deposited on a semiconductor substrate and bias voltage is applied between the electrodes as shown in Fig. 2.2 (a). When femtosecond laser pulses illuminate the gap between the electrodes on PCA, photo-carriers, Q_{photo} , are created and disappear like the plot in Fig. 2.2 (b). As a result, photo-carriers also flow with the same time behavior of Q_{photo} due to the applied bias voltage. Beause these photocurrents, J_{photo} , are again time-varing like the plot in Fig. 2.2 (b). THz waves, E_{THz} ,



Figure 2.2: Principle of T-ray generation in PCA. (a) Schematic illustration of T-ray generation from PCA. (b) Schematic time behavior plot of photo-carriers and photo-currents. (c) Schematic time behavior plot of T-ray radiation. From time-varying photo-currents, THz waves, E_{THz} , are radiated.

are radiated due to Maxwell's equations as

$$E_{\rm THz} \propto \frac{dJ_{\rm photo}}{dt}.$$
 (2.2)

The principle of the radiation is similar to usual antenna, so the name of them is photoconductive antenna.

For PCA, gallium arsenide (GaAs) is usually used as a semiconductor substrate because the bandgap of GaAs is lower than Ti:Sapphire laser photon energy and the life-time of photo-carriers in GaAs is short enough to raidate THz waves. The time scale of the existence of photo-carriers in GaAs is about 1 ps, so if one gives bias voltage between the electrodes, currents flow in about 1 ps time scale, then these time varying currents radiate electromagnetic waves of about 1 THz; THz waves radiate.

PCA is a very efficient THz emitter in low power laser systems. For high power laser systems, however, efficiency of it is reduced due to the saturation of photo-carriers. Large-area PCA [26] is one way to overcome this disadvantage. In this kind of PCA, photo-excitation area is about 1 mm², and the saturation occurs for much higher power laser pulses compared to that in typical PCAs. (The photo-excitation areas are usually less than 100 μ m² in usual PCAs.) The experimental demonstrations in Chapters 3 and 5 are performed with this large-area PCA.

2.3.2 Photo-Dember currents from low bandgap semiconductor

Diffusion currents in semiconductor are also used for THz wave generation, and just bare semiconductor wafers are usually used when one uses diffusion currents unlike drift currents in PCA.



Figure 2.3: Schematic diagram of photo-Dember currents near the surface of the semiconductor. Due to the mobility difference, net currents are built up.

The schematic diagram of photo-Dember currents near the surface of a semiconductor is shown in Fig. 2.3. When the femtosecond laser pulse illuminates on the surface of a semiconductor, photo-carriers are created and those carriers diffuse. At that time, net currents are induced because electrons diffuse much more compared to holes. This phenomenon is known as photo-Dember effect and the resulting electric current is photo-Dember current.

To generate high photo-Dember currents, the mobility difference between holes and electrons of the semiconductor should be large. In addition, the bandgap of the semiconducto should be low in order that photo-carriers can have high energy. Indium arsenide (InAs) satisfies these condition in 800 nm Ti:sapphire laser systems [27] and, therefore, InAs is the most popular one used to generate THz waves with the diffusion current method.

Photo-Dember currents are usually created toward semiconductor surface because photo-carriers are diffused inward to the semiconductor surface. However, by patterns on semiconductor surface, lateral direction currents can be generated [85]. This phenomenon is called as lateral Dember current and this phenomenon is used to generate polarization shaped THz waves in Chapter 4.

2.4 Detection of terahertz waves in THz-TDS

There are several ways to detect THz waves in THz-TDS, and coherent sampling in time domain with electro-optical crystal and PCA are common ways. We used electro-optical crystal in Chapters 3 and 5 while PCA is used in Chapter 4 in this dissertation, so we review these two ways in this section.

2.4.1 Electro-optical sampling

One way to detect THz waves is using the Pockels effect in non-linear crystals. The Pockels effect produces birefringence of non-linear crystals by an applied electric field on the crystal, and is distinguished from Kerr effect by the fact that the birefringence is proportional to the applied electric voltage. From this birefringence, the polarization of the transmitting light is rotated. As a result, because of the linearity between the field strength and the polarization rotation, one can maesure the amount of the field strength by maesuring the amount of polarization rotating. Because one uses the birefringence for polarization rotation, the non-linear crystal should be aligned in a proper angle to get more polarization rotation [28].

When THz waves and femtosecond laser pulses are propagating together in non-linear electro-optic crystals, femtosecond laser pulses feel THz pulses as DC electric voltage because the duration of femtosecond laser pulses is usually much shorter than the temporal field change of THz waves. As a result, by controlling the time interval between THz waves and femtosecond laser pulses, one can get THz time domain field shapes directly.

The most common non-linear crystal for electro-optical sampling is <110>-oriented zinc telluride (ZnTe) because of the phase matching condition in 800 nm Ti:sapphire laser systems [29, 30, 31]. Because the refractive indexes of ZnTe in THz frequency and in 800 nm are similar, THz waves and laser pulses are move together in quite longer distance than in other semiconductors. Therefore, the amount of polarization change is much bigger than that by other semiconductors. The disadvantage of ZnTe is its phonon-mode which is located in the frequency range between 3 THz and 7 THz [32]. As a result, higher frequency of THz waves is difficult to mearsure with ZnTe. To get higher frequency range measurement, gallium phosphide (GaP) is usually used instead of ZnTe.

Figure. 2.4 shows THz detection setup with electro-optical (EO) sampling. For the coupling of the THz waves and the femtosecond laser beam, a pellicle beamsplitter or a Si wafer is usually used as shown in Fig. 2.4, or indium tin oxide (ITO) coated glasses is also used in a bit diffetent setup [33]. Because we measure the amount of polarization rotation, the incident beam should be linearly polarized, so a polarizer is placed before the coupling of the THz waves and the femtosecond laser beam. The polarization of the linearly polarized laser beam is rotated in the EO crystal, and a quarter wave plate is placed after the EO crystal to compensate the bare polarization rotating from the EO crystal without THz waves. The amount of polarization rotation is measured by the balance detection with a Wollaston prism and two photo-detectors as show in Fig. 2.4 (a), or one photo-detector detection with another polarizer which composes the crossed polarizers with the first polarizer as show in Fig. 2.4 (b).



Figure 2.4: Schematic setup of THz detection with electro-optical sampling. (a) Balance detection setup. (b) One photo-detector setup.

2.4.2 Photoconductive antenna

One can also use PCA to detect THz waves as well as THz generation. When the femtosecond laser pulse illuminates on PCA, photo-carriers are created similarly as in the generation case. In the detection scheme, on the other hand, the bias voltage is not necessary. Instead of the bias voltage, THz waves themselves accelerate photo-carriers, then currents which are proportional to the THz field strength are made. From the measurement of these currents by controlling the time interval between THz waves and femtosecond laser pulses, THz field shapes can be detected.

Unlike PCA for THz generation, the photo-carrier life time in the semiconductor must be very short to get high resolution sampling because the sum of the photo-carrier lifetime and the duration of femtosecond laser pulses determine the time resolution. Therefore, low-temperature grown GaAs, of which the photo-carrier life time is less than 200 fs, is usually used for it.

2.5 Refractive index calculation in THz-TDS

To show an example of THz-TDS usages, we review the refractive index calculation from real data measured by THz-TDS in this section.

We draw schematic of a typical transmission type THz-TDS setup in Fig. 2.5. For the THz generation and detection, we draw our methods of this dissertation, and we note that these parts may be replaced by other methods, e.g. optical rectification for THz generation [22, 23, 24]. Off-axis parabolic mirrors or teflon lens are usually used for THz wave focusing and collimating, and a sample, of which one wants to measure the refractive index, is placed on at the focus of the THz-TDS.

In THz-TDS like Fig. 2.5, each transmitted monochromatic wave field through the sample, $E_{\text{sample}}(\omega)$, is expressed by [35],



Figure 2.5: Schematical drawing of a typical THz-TDS setup. For generation and detection, femtosecond laser pulses are used. We note that the emitter part and the detector part can be replaceable for proper purposes.

$$\frac{E_{\text{sample}}(\omega)}{E_{\text{Ref}}(\omega)} = \frac{2}{1+n} \frac{2n}{1+n} e^{i\frac{(n-1)\omega d}{c}},\tag{2.3}$$

where *n* denotes the refractive index of the sample, *d* denotes the thickness of the sample, *c* denotes the speed of light, and $E_{\text{Ref}}(\omega)$ denotes monochromatic wave field without the sample. In Eq. 2.3, the first two terms express Fresnel coefficients, and the exponential term means the phase propagation in the sample. It is noted that *n* is generally the complex number and the etalon effect is ignored in Eq. 2.3. Assuming the absorption of the sample is small, Fresnel coefficients, $\frac{2}{1+n}\frac{2n}{1+n}$, can be treated as real numbers and, as a result, it doesn't affect the phase of the signal. With this assumption, the phase difference, $\Delta\phi$, satisfies

$$\Delta \phi = \phi_{\text{sample}} - \phi_{\text{ref}} = \frac{(n-1)\omega d}{c}, \qquad (2.4)$$

where ϕ_{sample} denotes the measured phase with the sample while ϕ_{ref} denotes the measured phase without the sample. Therefore, the refractive index of the sample is easily obtained by

$$n = 1 + \frac{c\Delta\phi}{\omega d}.\tag{2.5}$$

The real data is shown in Fig. 2.6. Undoped silicon wafer, 500 μ m thick, is used as the sample for Fig. 2.6. Measured time domain signals with and without the silicon wafer are shown in Fig. 2.6 (a)

and corresponding spectrums are in Fig. 2.6 (b). As we mentioned in previous sections, THz waves in THz-TDS have sub-cycle nature and ultra-broad bandwidth as shown in Figs. 2.6 (a) and (b).

Transmission of the sample, $\left|\frac{E_{\text{sample}}(\omega)}{E_{\text{Ref}}(\omega)}\right|$, is easily calculated from Fig. 2.6 (b) and shown in Fig. 2.6 (c). The sawtooth-like behavior of the transmission comes from the etalon effect [36]. Because of ultra-broad bandwidth, the transmission is achieved in very wide frequency range in THz-TDS.

The refractive index calculation process is following: The phase differences in Eq. 2.4 are obtained from phases of Fourier transformed signals, and they are plotted in Fig. 2.6 (d). However, information in Fig. 2.6 (d) can not be used to calculate the refractive index of the sample yet because phases are wraped between $-\pi$ and π . Fortunately, this 2π ambiguity can be removed with the ultra-broad spectrum of THz waves because the phase diffrences of very low frequencies should be between $-\pi$ and π regardless of the 2π ambiguity due to Eq. 2.4 and the phase diffrences of higher frequencies can be determined by these phase information of low frequencies. The phase diffrences in Fig. 2.6 (e) is obtained from this phase unwrap process, and the refractive indexes calculated from phase information in Fig. 2.6 (e) is shown in Fig. 2.6 (f). The line in Fig. 2.6 (f) has sawtooth-like shape because we ignore the etalon effect. There are some methods to remove this artificial effect [37, 38], but we skip these methods in this dissertation.



Figure 2.6: Refractive index calculation process with THz-TDS for silicon wafer. (a) Time domain signals with and without silicon wafer. (b) Corresponding spectrums. (c) Transmission calculated from (b). (d),(e) Calculated phase differences in the frequency domain (d) and unwraped phase differences (e). (f) Calculated refractive index of Si wafer.

Chapter 3. Single-pixel broadband diffraction imaging

Imaging is one of the most important research topics in optics and diffraction imaging is also an important research topic in Fourier optical application. In diffraction imaging, coherent light illuminates an image target and is diffracted by the image target. In far field condition, the diffracted light has the amplitude and phase profile just as Fourier transform of the image target. Therefore, if one gets this Fourier transformed information in far field, original image information of the image target can be obtained by Fourier transform: this is the basic principle of diffraction imaging.

If one perform a diffraction imagery with THz-TDS system, direct phase measurement and ultrabroad bandwidth, which we emphasize in Chapter 2, give great advantages. With direct phase measurement, phase retrieval processes are not necessary as against visible light diffraction imaging. Ultra-broad bandwidth gives even better advantage; Raster scanning or 2 dimensional detectors usually seems to be essential to get 2 dimensional information, but it doesn't with ultra-broad bandwidth THz waves. In the following sections, we show these advantages in more detail and demonstrate three different single-pixel imagery which use the ultra-broad bandwidth nature of THz waves.

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3.1 Main concept

3.1.1 Advantage from direct phase measurement

In diffraction imaging, both Fourier transformed spectral phase and amplitude information are naturally essential. However, relatively, the spectral phase information is more important than the amplitude information. To see it, we show an example in Fig. 3.1. The original picture, which denotes peoples who mostly help this dissertation, is in Fig. 3.1(a), and the Fourier transformed amplitude and phase information of the picture are shown in Figs. 3.1(b), (c). Figs. 3.1(d),(e),(f) represent reconstructed images with only amplitude information, only phase information, and both amplitude and phase information, respectively. As show in Fig. 3.1, the image in Fig. 3.1(e) shows the shape of the original image in Fig. 3.1(a) while the image in Fig. 3.1(d) shows nothing.

Nevertheless, acquisition of phase information is not straightforward in usual diffraction imaging. If one uses visible light as the light source in diffraction imaging, the Fourier transformed phase information is usually not able to be obtained because there is not direct phase detector in visible light frequency. Therefore, phase information of diffractive waves must be retrieved by phase retrieval algorithms, such as Gerchberg–Saxton algorithm [39].

On the other hand, in THz diffraction imaging, one can obtain both amplitude and phase information simultaneously as shown in Chapter. 2. As a result, phase retrieval algorithms are not necessary in THz diffraction imaging. This is the first advantage of diffraction imagery with THz-TDS system.



Figure 3.1: (a) Original picture. (b) Amplitude information in Fourier domain. (c) Phase information in Fourier domain. (d) Reconstructed image with only amplitude information. (e) Reconstructed image with only phase information. (f) Reconstructed image with both amplitude and phase information.

3.1.2 Advantage from ultra-broad bandwidth

The second advantage of THz waves for diffraction imaging is its ultra-broad bandwidth. THz waves have ultra-broad bandwidth, the frequency-to-bandwidth ratio of near unit, and this property can omit 1-dimension scanning in data acquisition. This idea is the major concept of this chapter.

In diffraction imaging, getting Fourier transformed information with raster scan in the spatial frequency domain or use 2-dimension detectors, such as CCD camera, is common way. In such a process, the light frequency is usually treated just a constant. However, image systems based on THz-TDS have extreme broad bandwidth, frequencies can be one axis of variables. In other words, Fourier images from multi frequencies are just similar, so radial direction raster scanning is not necessary using extreme broad bandwidth light.

For simplicity, let us consider 1-dimension case first. We draw the schematic concept in Fig. 3.2. When the coherent wave is illuminated on an image target, U(x), the diffracted electric field, V(k, X),



Figure 3.2: Concepts of (a) conventional diffraction imaging with monochromatic waves and (b) singlepixel diffraction imaging with extreme broadband waves

is expressed as

$$V(k,X) = \frac{ke^{ikz}}{i2\pi z} \int U(x)e^{ikxX/z}dx,$$
(3.1)

where k is wavenumber and z is the distance between aperture and spatial frequency plane. To get the information of V(k, X), raster scanning on X is essential like Fig. 3.2(a). However, if ultra-broadband waves are used, each frequency signal represents one point signal in the spatial frequency domain, so one dimensional information is automatically acquired by spectral analysis like Fig. 3.2(b). As a result, raster scanning on X is not necessary.

Let us consider 2-dimension case for real applications. In 2-D case, the diffraction field, V(k, X, Y), becomes as

$$V(k,X,Y) = \frac{ke^{ikz}}{i2\pi z} \int U(x,y)e^{ik(xX+yY)/z}dxdy = \frac{ke^{ikz}}{i2\pi z} \int U(x,y)e^{ikR(x\cos\theta+y\sin\theta)/z}dxdy, \quad (3.2)$$

where $R = \sqrt{X^2 + Y^2}$ and $\theta = \tan^{-1} \frac{Y}{X}$. According to equation. 3.2, the wavenumber, k, can replace R, so 2-D information can be acquired by spectral analysis and 1-dimensional angular direction information. It is noted that 1-dimension data acquisition is still needed, and following three sections are about how we collect this angle information.

Scanning dimension reduction is practically important because conventional THz imaging system is very primitive. Most of the conventional THz imaging is based on a simple raster scan using mechanical delays, so the acquisition speed is one of the limiting factor in real application. To overcome this, 2D electro-optic imaging [40], THz detectors array [41], and reciprocal imaging [42] technique has been proposed at the cost of high implementation complexity. Recently, Chan et. al. [43, 44] has employed a compressed sensing (CS) [45] technique in signal processing community for THz-imaging. In their works, using only a single detection and intelligent choices of spatial modulation, they reduced the image acquisition time significantly. However, those works were mainly based on THz-intensity measurement rather than exploiting the extremely broad band nature of THz-spectrum. It is now well known that the broad band THz signal can be reliably measured using THz-TDS. Furthermore, fast waveform measurement is under investigation by many groups [46], for which mechanical scanning is now being replaced by electro-optical scanning skill as phase locked THz-asynchronous optical sampling(AOS) [47, 48]. Therefore, the application goal of the broadband diffraction imaging is to exploit the extremely broad bandwidth of THz signal to drastically reduce the number of samples; hence, to accelerate the acquisition time.

3.2 Single-pixel diffraction imaging with coherent optical computer

3.2.1 Introduction

Coherent optical computer, or 4F-correlator, deals with acquisition of information carried by electromagnetic waves and has found many applications in image and signal processing [36, 49]. The basic operation is setting the double-Fourier transform optical systems with transform optics, such as lens, and Fourier filters, M(X, Y) to set the relation of an object, U(x, y) and an image v(x', y') as

$$V(x', y') = F[M(X, Y) \times F[U(x, y)]],$$
(3.3)

where F represent the Fourier transform. This well-known relation between the object and image is usually defined for a monochromatic wave.

In this section, a single pixel THz imaging system is proposed by exploiting ultra-broad bandwidth of THz-TDS pulses. In the proposed system, a collimated THz beam is illuminated on a targets and the scatted fields are measured through a hole at the Fourier plane using a coherent optical computer. This setup allows conversion of temporal spectrum of THz-pulse to a radial spatial frequency spoke in Fourier domain. Hence, 2-D image can be readily obtained by rotating a hole around an optical axis. Experimental results confirm that a complicated object can be reliably obtained using only 30 waveform measurements.

3.2.2 Theory

This idea can be explained using Fourier optics theory [50]. The target object is placed at an image (x, y) plane, and illuminated by collimated terahertz pulses as shown in Fig. 3.3. The scattered field from the object is then collected by transform optic and is propagated to the spatial frequency plan (X, Y). In the spatial frequency domain, a hole mask is placed such that it samples a specific spatial frequency, which is then measured by a detector, electro-optic sampling using ZnTe thin film in this case.

As the mask M(X, Y) is located at the far field, the detector measurement through the mask on the Fourier plan can be represented by y(k):

$$V(k) = S(k) \left(\frac{k}{i2\pi f}\right)^2 \int M(X,Y) \left[\int U(x,y) e^{\frac{-ik(xX+yY)}{f}} dx dy\right] dX dY$$
(3.4)

where S(k) is the spectrum of the emitter, U(x, y) is the object, f is the focal length, and $k = \frac{2\pi}{\lambda}$ is the wavenumber, respectively. Furthermore, the spectrum of the emitter, S(k), can be readily measured using the same setup without the object and the mask.

If the mask is composed of an infinitesimal hole at distance d with angle θ ; i.e. $M(X, Y) = \delta(X - d\cos\theta, Y - d\sin\theta)$, the equation (3.4) can be simplified as

$$V(k,\theta) = S(k)\left(\frac{k}{i2\pi f}\right)^2 \int U(x,y)e^{\frac{-ikd}{f}(x\cos\theta + y\sin\theta)}dxdy.$$
(3.5)

Using the Fourier slice theorem [51], the inverse Fourier transforms of $\frac{V(k,\theta)}{S(k)} (\frac{i2\pi f}{k})^2$ provides as

$$P(u,\theta) = \int U(x,y)\delta(x\cos\theta + y\sin\theta - \frac{fu}{d})dxdy$$
(3.6)

which corresponds to the projection of the image on the θ direction, or sinogram. Therefore, one can recover original image U(x, y) using inverse Radon transformation, if one can collect measurement for sufficient number of $\theta's$ by rotating the hole.

In the real experiment situation, the hole has nonzero radius a as shown in Fig. 3.3, so the equation (3.6) can be replaced by,

$$P(k,\theta) = \frac{\pi a^2}{4} \int U(x,y) \frac{2J_1(ka\rho/2f)}{ka\rho/2f} e^{\frac{-ikd}{f}(x\cos\theta + y\sin\theta)} dxdy$$
(3.7)

where $\rho = \sqrt{x^2 + y^2}$, and J_1 represents the first order bessel function of the first kind, respectively. This Bessel term correction results in distortion to the reconstructed image and determines the imaging fieldof-view(FOV). For example, the imaging FOV is limited as $\rho < \frac{4.43f}{k_{max}a}$, which satisfies $\frac{2J_1(ka\rho/2f)}{ka\rho/2f} > \frac{1}{2}$ where k_{max} denotes the maximum wavenumber in the imaging process. This implies that the FOV is inversely proportional to k_{max} . Furthermore, the image resolution of our system is determined by the maximum spatial frequency, which is proportional to the distance to the hole, d. With a simple calculation, it can be shown that the image resolution is given by $\frac{k_{max}d}{F}$. Hence, the larger d and the smaller a provide better image reconstruction at the expense of SNR loss. On the other hand, the longer focal length F is good for FOV although bad for image resolution.

3.2.3 Experimental description

In the experimental setup, we used 100 MHz, 350 mW, 50 fs Ti:sappire oscillator system. Large area PCA [26] and < 110 >-oriented 1 mm ZnTe are used as an emitter and a detector. The mask has a 5 mm diameter hole, which is 15 mm apart from the optical axis. Parabolic mirrors with f = 150mm are used for collimating emitted terahertz pulse and propagating to the mask, and a parabolic mirror with f = 100mm is used for focusing to the detector. Shorter focal length focusing mirrors are usually preferred due to the tight focusing and a large NA. Although we use two different focal length parabolic mirrors, the principle is the same and our analysis still holds. Spectrums up to 1.5 THz frequency signals use for imaging process. The frequency interval is given by about 0.01 THz.

3.2.4 Results

Experimental results are shown in Fig. 3.4. Fig. 3.4.(a) represents the target object that represents "light" in Korean, whose dimension is about $2 \text{cm} \times 2 \text{cm}$. The hole mask has 5mm diameter hole and is apart 15mm from the center of the mask. Entire target was illuminated, using a collimated THz pulses,



Figure 3.3: (a) Experimental setup for single-pixel diffraction imaging with coherent optical computer. (b) The mask geometry.



Figure 3.4: Experimental results. (a) Imaging target. (b) Measured time signals. (c-f) Reconstructed image with 6 waveforms (c), 10 waveforms (d), 15 waveforms (e), and 30 waveforms (f).



Figure 3.5: Experimental results. (a, c) Imaging targetes. (b),(d) Reconstructed images with 18 waveforms from (a) and (c), respectively.

and the available FOV is $\rho \leq \frac{4.43f}{k_{max}a} \sim 1.1$ cm, so this target satisfied the FOV condition. We uniformly sampled 30 waveforms in 0 ~ 180 degree as shown in Fig. 3.4.(b). Reconstructed images are shown in Figs. 3.4(c)-(f). We choose 6, 10, 15, and 30 waveforms with equal spacing in 0 ~ 180 degree for reconstructing the image, respectively. Using only 30 waveforms, we have reasonable quality images.

Other Experimental results with similar experimental conditions are shown in Fig. 3.5. Fig. 3.5.(a) represents a target object that represents a pictogram of Taekwondo, and Fig. 3.5.(b) shows its reconstructed image with 18 waveforms. Fig. 3.5.(c) represents the other target object, which is an earring, and Fig. 3.5.(d) shows its reconstructed image with 18 waveforms. We could also get reasonable quality images as the results in Fig. 3.4.

3.2.5 Discussion

The imaging principle might be equivalently stated using time-of-flight (TOF) view point under geometric optics approximation and the assumption that the illuminated pulse is the delta function in time. We draw this concept in Fig. 3.6. Note that at a specific time point, the scattered field from the equidistance TOF line arrives at the hole simultaneously. Hence, the measurement at the hole is the line integral along the equal TOF line. For different time point, the equal TOF line is varying. Hence, the time trace of the measurement at the hole represents the projection data along different radial distance



Figure 3.6: The schematic drawing of time-of-flight analysis for the same measurement. By the lens, the scattered fields along the line, which are perpendicular to θ , have the same optical path length to the hole. Therefore, the projection of the image is acquired by wave trace measuring.

at angle θ .

Sampling number might be even more reduced in more developed setups. First, the time separating mask could be used instead of a hole mask as shown in Fig. 3.7(a). Terahertz transmitted material such as silicon could be placed azimuthally with different thickness in this mask. In this particular setup, terahertz waves arrive to the detector separately in time and each separated wave can be used for the image reconstruction process. As a result, one waveform diffraction is even possible. This concept is realized in chapter 3.3.

On the other hand, detector array are arranged azimuthally as shown in Fig. 3.7(b). Putting the detector array in the spatial frequency domain instead of the hole mask, 2D image can be archived by 1D detector array only.

The main disadvantage of the system is low SNR, since the hole mask blocks almost whole terahertz pulse. However, automatic repetition of pulse measurement using THz asynchronous optical sampling [47, 48] or more powerful sources may make the SNR sufficiently large for real time measurement. In addition, there might be mask-less single-pixel diffraction imaging, which is free from the bad SNR. We will explain it in Section 3.4.

3.2.6 Summary

In summary, we have demonstrated the single-pixel imagery of objects by exploiting the extreme broadband nature of ultrafast THz pulses. In this newly developed coherent optical computing scheme for a broadband source, 2D spatial information can be encrypted into waveforms, or a single waveform, and the image is recovered through inverse radon transformation. The THz imaging problem is now converted to 1D scanning rather than 2D one, which may significantly accelerate the acquisition time.



Array Detector

Figure 3.7: More developed schemes of single-pixel diffraction imaging with coherent optical computer.(a) One waveform diffraction imaging from time separation. (b) Detection array concept.

3.3 One waveform imaging

3.3.1 Introduction

It is worth noting that the imaging methods in the previous chapter 3.2 used *active* masking for 2D imaging. This method requires the measurement of N different waveforms, each containing specific angular projection information of the object. Mathematically there may exist a number of techniques that permit the extraction of complete spatial information for a 2D object from a single waveform. The simplest method is the use of a single Fourier-domain mask [Fig. 3.7(a)] constructed with N holes of various phase retardations. This Fourier mask, used in a coherent computational setup in the previous setup, temporally separates N THz waveforms, each containing individual angular object information with respect to each other. Then, a single time-domain scan of the diffracted THz wave simultaneously records the complete angular projection image of the 2D object, and therefore, a 2D image recovery from a single THz waveform might be achieved.

3.3.2 Experimental description and results

Experimental setup is just same as the previous chapter 3.2 except the mask part. In this experiment, the mask has 12 holes with 6mm-diameter which are 15mm apart from the optical axis as shown in Fig. 3.8(a). Silicon blocks with different thicknesses are glued the mask together on hole positions. The time interval of the separated signals is about 8ps by the silicon blocks. Fig. 3.8(b) represents the target object, whose dimension is about 1cm × 1cm. In this setup, the available FOV is $\rho \leq \frac{4.43f}{k_{max}a} \sim 0.8$ cm, so the target is small enough to be seen. The measured waveform is plotted in Fig. 3.8(c). We separate this waveform into 12 waveforms and waveform separating is indicated by dash lines in Fig. 3.8(c). The reconstructed image and overlapped image with the target is shown in Fig. 3.8(d) and (e), respectively. Recognizable image is also achieved as the results in the previous section from only a single waveform.

3.4 Single-pixel diffraction imaging with a slanted phase retarder

In this section, we demonstrate single-pixel diffraction imaging, whereby broadband terahertz (THz) waveforms passed through a slanted phase retarder (SPR), instead of a hole mask, diffracted from an object, were measured by a THz detector located in the far field. For 1D imaging, the fixed-location single-pixel broadband detector simultaneously measured all the spatial frequency components of the object because the frequency components of the source maintain a one-to-one correspondence with the object's spatial frequency. For 2D imaging, the angular position of the SPR enabled the diffracted THz wave to carry an angular projection image of the object. Thirty waveforms are measured at different SPR orientations to reconstruct complex 2D images.

3.4.1 Introduction

Coherent diffraction imaging (CDI) is an image reconstruction technique for small-size objects using highly coherent optical, X-ray, or electron beams, in which a real-space image is reconstructed from a diffraction pattern collected by a detector array via an iterative feedback algorithm [52]. Recently developed high-energy photon sources permit CDI of nanoscale structures, such as nanotubes, quantum



Figure 3.8: Summary of one waveform diffraction imaging. (a) Time separating mask. (b) The image target. (c) The measured waveform. Dash lines indicate time separation. (d) Reconstructed image. (e) Overlapped image with image target.
dots, and possibly proteins [53, 54, 55]. Also, CDI with optical waves has proven useful in obtaining tomographic high-resolution images of live cells [56]. The image resolution of CDI depends on the wavelength and the extension of the measured diffraction pattern. For a monochromatic wave of wavelength λ , the Fraunhoffer diffraction pattern V(X) of an object U(x) is

$$V(X) = \frac{e^{ikz}e^{i\frac{kX^2}{2z}}}{i\lambda z} \int U(x)e^{-i\frac{2\pi}{\lambda z}xX}dx,$$
(3.8)

where x and X represent spatial coordinates in the real and reciprocal spaces, respectively, k is the wave number, and z is the distance from the object to the detector. The Fourier component of U(x) evaluated at spatial frequency $f_X(=X/\lambda z)$, that is $\tilde{U}(f_X)$, is captured in V(X), aside from the given phase factor. For a high-resolution image of maximum spatial frequency f_{\max} , an array detector of lateral size $X_{\max} = \lambda z/f_{\max}$ is required.

However, given a broadband coherent source with a frequency distribution ranging from zero to $\omega_{\max}/2\pi$, a single-pixel detector can replace the detector array because the frequency components of the source maintain a one-to-one correspondence with the spatial frequency components of the object. The point detector placed in a fixed position X_o can simultaneously measure all the Fourier components of U(x); therefore, single-pixel imaging can be achieved such that

$$U(x) = \int_0^{\omega_{\max}} \tilde{U}(f_{X_o}; \omega) e^{-ixf_{X_o}(\omega)} d\omega, \qquad (3.9)$$

where ω is the angular frequency and $\omega_{\text{max}} = 2\pi c f_{\text{max}} z/X_o$. In this proposed method for single-pixel coherent diffraction imaging (SP-CDI), the spatial resolution is limited by the frequency maximum ω_{max} of the coherent source, not by the detector size.

For a broadband coherent source, we consider ultrafast THz pulses [57]. A typical THz pulse frequency range for THz time-domain spectroscopy (THz-TDS) is 0 to 3 THz [58] and a record broad bandwidth of 80 THz has been reported [59]. They have an extremely broad range of frequency components with a characteristic frequency-to-bandwidth ratio near unity. Conventional use of ultrafast THz waves in imaging involves a raster scan to move an object around a tightly focused THz beam [60] and this method has a diverse range of imaging applications extending from semiconductors and metal structures to biological and medical objects [61, 62, 63]. However, due to the limitation of the data acquisition speed of this mechanical scanning method, various alternatives have been proposed, including 2D electro-optic imaging [64], a focal-plane detector array [65], and compressed sensing techniques [43, 44], at the cost of implementation complexity. In the previous section, we demonstrated coherent optical computation for single-point THz imaging, where an active Fourier mask in a conventional THz-TDS setup converted a 2D image into N temporal waveforms. In this section, using a completely different approach, we propose single-pixel detection of coherent diffraction images and demonstrate various 2D image reconstructions.

3.4.2 Theory

In SP-CDI, a target 2D object is placed in the object plane $\Sigma_o(x, y)$, as shown in Fig. 3.9(a), and illuminated by collimated THz waves. The diffracted field from the object U(x, y) is then collected by a THz detector located at the center of the far-field diffraction plane $\Sigma_d(X, Y)$, i.e., X = Y = 0. To redirect all the spatial frequency components to the detector location, a slanted phase retarder (SPR), shown in Fig. 3.9(b), is inserted in front of the object. For an incident THz wave of spectral field profile



Figure 3.9: Experimental setup and geometry. (a) Schematic of single-pixel diffraction imaging with SPR. (b) Slanted phase retarder (SPR). (c) Illustration of beam deviation.

 $S(\omega)$, the diffracted field $V_{\theta}(\omega)$ is given by

$$\frac{V_{\theta}(\omega)}{S(\omega)} = \frac{e^{ikz}}{i\lambda z} \int_{\Sigma_o} U(x, y) e^{ik(x\cos\theta + y\sin\theta)\sin\phi} dxdy,$$
(3.10)

where θ is the angular position of the SPR and ϕ denotes the deviation angle of the beam through the SPR, as shown in Fig. 3.9(c). Due to the angular orientation of the SPR, the diffracted THz wave carries an angular projection image of the object. Using a procedure that is mathematically similar to the method described in the previous section, the original object U(x, y) is recovered from a number of measurements carried out at different θ s by

$$U(x,y) \propto \mathcal{R}_{\theta}^{-1} \left[\mathcal{F}^{-1} \left[\frac{V_{\theta}(\omega)}{\omega e^{ikz} S(\omega)} \right] \right], \qquad (3.11)$$

where $\mathcal{R}_{\theta}^{-1}$ and \mathcal{F}^{-1} are inverse Radon and inverse Fourier transformations, respectively.

3.4.3 Experimental description and results

For the experiment, we used a Ti:sapphire laser oscillator that produced IR short pulses at an average power of 350 mW. THz waves were generated from a large-area photoconductive antenna (PCA) [66] and then collimated by an off-axis parabolic mirror with a 150-mm focal length. For detecting the diffracted THz waves, a 2-mm-thick ZnTe electro-optic crystal was placed in the front focal plane of another parabolic mirror with a focal length of 100 mm. Time-resolved THz electric field measurements



Figure 3.10: Experimental results. (a) Image target. (b) Measured waveforms. (c) Reconstructed image. (d) Sharpened image by high-frequency pass filtering of measured waveforms in (b).

were carried out by mapping the polarization changes of optical gate beams, due to the Pockels effect induced in the electro-optic crystal by the electric field of the THz pulse [30].

The object, a representation of a feline paw shown in Fig. 3.10(a), was made from a 0.5-mm-thick metal plate of area 2 cm \times 2 cm. The SPR was made out of polytetrafluoroethylene (Teflon) and had a cylindrical shape (radius 25 mm) cut at an angle $\alpha = 15^{\circ}$. The index of refraction of Teflon is a constant n = 1.46 over the THz spectral range.

The procedure for data collection and image recovery was as follows. First, both the object and the SPR were temporarily removed and the reference THz field spectrum at the detector, $S_d(\omega)$, was obtained by taking the Fourier transform of a THz time-domain signal. It is noted that $S_d(\omega)$ differs from the THz field spectrum at the object by a factor of ω , aside from a constant factor. Then, the object and the SPR were replaced and N = 30 different THz waveforms were measured at various angles uniformly sampled from $\theta = 0^{\circ} - 180^{\circ}$. [Fig. 3.10(b)] The time-domain waveforms were recorded with a spectrum of up to $\omega_{\text{max}} = 1.5$ THz with a resolution of 0.03 THz. By following the signal processing described in Eqs. (3.10) and (3.11), the coherent diffraction image was retrieved. [Fig. 3.10(c)] Owing to the oneto-one correspondence of the THz frequency to the image spatial frequency, the Fourier synthetic image processing can be implemented in a variety of ways by directly manipulating the Fourier components of the THz waveforms. For example, a sharpened image, such as that in Fig. 3.10(d), was obtained via high-pass filtering of measured THz waveforms.

Same procedure is also possible when the SPR is placed in the back of an image target. To verify this, we place the SPR in the back of an image target and measure waveforms as we did for Fig. 3.10. The geometrical configuration is shown in the inset figure in Fig. 3.11.(a). The imaging target is shown in Fig. 3.11.(a) and the reconstructed image is shown in Fig. 3.11.(b). To reconstruct the image, we measure 15 waveforms with 12 degree spacing. Imaging is well done as the result shown in Fig. 3.10.

3.4.4 Image resolution

The SP-CDI image resolution is not directly related to the numerical aperture or the focal length of the diffractive optic. Instead, the beam deviation angle ϕ is a scaling coefficient between f_{max} and ω_{max} , i.e., $f_{\text{max}} = \omega_{\text{max}} \sin \phi / 2\pi c$, and therefore, determines the image resolution. Figure 3.12 shows the result of an imaging experiment with an object of a double-slit pattern. For 1-mm hole double slits separated by 2 mm, as shown in Fig. 3.12(a), three different SPRs cut at $\alpha = 10^{\circ}$, 20° , and 30° were used, and the diffraction images shown in Fig. 3.12(b)-(d), respectively, were obtained. The SPR angles were chosen to give image resolutions of $1/f_{\text{max}} = 2.4$, 1.2, and 0.7 mm, respectively, and as expected, the double-slit patterns were resolved in Figs. 3.12(c) and (d) only. For enhanced image resolution, larger SPR angles should be considered. However, from the relationship $\phi = \sin^{-1}(n \sin \alpha) - \alpha$, total internal reflection will occur in the SPR and the image resolution is limited as

$$\frac{1}{f_{\max}} = \frac{\lambda_{\min}}{\sin \phi} \le \frac{n}{\sqrt{n^2 - 1}} \lambda_{\min}, \qquad (3.12)$$

where λ_{\min} is the minimal wavelength of the given THz pulse. Figure 3.12(e) compares the measured maximal frequencies with Eq. (3.12): The calculated f_{\max} from the images are shown in dots and the the result from Eq. (3.12) in a red line. Both, plotted as a function of the SPR angle α , show a good agreement. As a result, the resolution limit in SP-CDI is determined by both the index of refraction of the SPR and the maximal THz frequency. In the ideal case, the resolution of SP-CDI is about λ_{\min} due to the limit of wave propagation like usual light microscopy.

3.4.5 Discussion

SP-CDI can be implemented using broadband waves in different frequency ranges. For example, sub-femtosecond pulses produced via high harmonic generation of an ultrashort infrared pulse in atoms encompasses the whole spectral range of visible and UV/XUV [67]. Another candidate is the supercontinuum formed as a result of cascading nonlinear processes of IR short pulses, as seen, for example, in a photonic bandgap fiber, which spans several optical octaves with a spectral range extending from UV to beyond mid-IR [68]. Both broadband sources are capable of SP-CDI given a proper choice of diffractive optics. With these higher frequency waves as a source, proper phase retrieval process might be needed.

3.4.6 Summary

In summary, we demonstrated coherent diffraction imaging using a fixed-location single-pixel detector. The broadband nature of the THz waves was used for one-to-one mapping of the spatial frequency of





Figure 3.11: Imaging results with the SPR which is placed behind the image target. (a) Imaging target. (b) Reconstructed image with 15 waveforms.



Figure 3.12: (a) Image resolution target. (b)-(d) Reconstructed images with SPRs at $\alpha = 10^{\circ}$ (b), 20° (c), and 30° (d). (e) Maximum spatial frequency f_{max} (in λ_{\min} unit) plotted as a function of SPR angle α . The blue line denotes silicon SPR while the red line denotes Teflon SPR in (e).

an object to the frequency of the diffracted waves, and by adopting a slanted phase retarder, a fixed-point single detector collected complete 2D angular projection images of various objects, enabling single-pixel 2D coherent diffraction imaging. Our proposed idea could eliminate the need for area detection in coherent diffraction imaging.

Chapter 4. Polarization shaping of few-cycle terahertz wave

In this chapter, we present a polarization shaping technique for few-cycle terahertz (THz) waves. For this, N femtosecond laser pulses are generated from a devised diffractive optical system made of as-many glass wedges, which then simultaneously illuminate on various angular positions of a sub-wavelength circular pattern of an indium arsenide thin film, to produce a THz wave of tailor-made polarization state given as a superposition of N linearly-polarized THz pulses. By properly arranging the orientation and thickness of the glass wedges, which respectively determine the position and timing of the femtosecond laser pulses, we successfully generate THz waves of various unconventional polarization states, such as polarization rotation and alternation between circular polarization states.

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4.1 Introduction

Ultrafast pulse shaping technique has enabled on-demand generation of visible light of arbitrary waveforms, making significant contributions in many research areas including laser spectroscopy [69], quantum control of non-linear processes [70], and magnetic spin state control [71], to list a few. Among the many degrees of freedom of light, polarization has been the least under consideration. In recent years, however, polarization has gradually become an important control parameter, and the polarization state shaping of optical frequency wave, which has been pursued with the help of well-developed optical devices and components, such as optical gratings, or liquid crystal devices [72], is successfully applied for spintronics [73] and photo-biochemistry [74].

What about THz frequency wave? Recently, this undeveloped frequency region has attracted a great deal of interest [75, 76]. THz frequency waves of controlled polarization state are relevant in use for many fundamental studies: Not to mention the rotational motions of aqueous molecules, but also various material waves, for example, the spin wave of magnetic materials or the vibrational waves of circularly dichroic biological molecules belong to this frequency region [77, 78, 79]. Additionally THz-frequency communication is another attractive issue, where the polarization synthesis may play an as important role as in radio-frequency communications [80]. There have been attempts to achieve the circular polarization of THz frequency waves by combining a couple of linearly-polarized THz waves [81], or by passive optical components, such as prisms [82], Fresnel rhombs [83], achromatic wave plates [84]. Yet, the scope of THz-version of polarization state shaping is rather limited to a few simple polarization states.

In this chapter, we present an idea of polarization state shaping for arbitrary waveform synthesis for THz frequency waves, inspired by the recent work carried out by Klatt and co-workers [85]. According to their report, the photo-Dember current injected by a femtosecond laser pulse that illuminates on a metal-semiconductor interface flows perpendicular to the interface, and, as a result, the THz wave radiated in the direction of the surface normal is linearly-polarized, perpendicular to the direction of

the interface. We can then use a circular interface between the semiconductor and metal to generate THz wave linearly-polarized along an arbitrary direction. With this method, then multiple THz waves simultaneously generated from different locations of the circular interface can be superposed to make a polarization shaped THz wave.

In the subsequent sections, after introducing a new definition for the polarization state of fewcycle THz pulses, we present an experimental demonstration of THz polarization synthesis technique. Diffractive optical systems are devised being made of N glass wedges (N=4 or 6), which are used to produce the properly arranged as-many optical pulses in time and space. When a femtosecond laser pulse passes through one of the diffractive optical systems, a set of laser pulses arranged in time and space is produced, which then illuminates a sub-wavelength InAs thin film to produce THz waves of tailor-made polarization states. After the proof-of-principle experiments, a short discussion of the validity of this polarization shaping technique follows.

4.2 Polarization representation for few-cycle THz waves

The nature of non-linear polarization of few-cycle or sub-cycle waves differs from the well-known behavior of monochromatic or quasi-monochromatic waves [83]. As such extremely short pulses consist of a broad range of spectral components, the slowly-varying envelope approximation, which is the presumption for the conventional polarization representations, including Jones vector, Stokes vector, and Poincaré sphere representations, is not adequate. Note that the Jones vector representation uses the phase delay between two linear polarization components, defined as a function of a carrier frequency; and that the principal axes and the polarization ellipticity in Poincaré representation make no sense if the polarization changes significantly in one cycle of oscillation.

In order to properly describe the polarization state of a few-cycle pulse, therefore, a new definition for polarization ellipticity is needed, without relying on the slowly-varying envelope approximation and strictly given in terms of its constituent linear-polarization components in time domain. Suppose an electric field is given as a superposition of two orthogonal fields, $\hat{x}E_x(t)$ and $\hat{y}E_y(t)$, linearly polarized along the x- and y-axes, respectively, We may then define the amplitude of its right-circularly polarizated component, $\tilde{E}_R(t)$, and the amplitude of its left-circularly polarized component, $\tilde{E}_L(t)$ as

$$\tilde{E}_{R,L}(t) = \frac{1}{\sqrt{2}} (\tilde{E}_x(t) \pm i \tilde{E}_y(t)), \qquad (4.1)$$

where $\tilde{E}_{x,y}(t)$ are the complex amplitudes, given from Hilbert transformation of $E_{x,y}(t)$ [86]. These defined parameters satisfy $\tilde{E}_x(t)\hat{x} + \tilde{E}_y(t)\hat{y} = \tilde{E}_R(t)\hat{\varepsilon}_R + \tilde{E}_L(t)\hat{\varepsilon}_L$ where the resulting unit vectors $\hat{\varepsilon}_R = (\hat{x} - i\hat{y})/\sqrt{2}$ and $\hat{\varepsilon}_L = (\hat{x} + i\hat{y})/\sqrt{2}$ denote the right- and left-circular polarizations, respectively, as in Johns vector representation [36].

In Poincaré sphere representation [87], the angle of polarization ellipticity is determined by the ratio of the semi-major and semi-minor axes of an electrical field ellipse. For a monochromatic wave, the semi-major axis is the sum of the absolute values of the right- and left-circular polarization amplitudes, and the semi-minor axis is the difference between them. In this regard, we may newly define the polarization ellipticity ε without a loss of generality as

$$\varepsilon(t) = \tan^{-1}\left(\frac{\left|\tilde{E}_{L}(t)\right| - \left|\tilde{E}_{R}(t)\right|}{\left|\tilde{E}_{L}(t)\right| + \left|\tilde{E}_{R}(t)\right|}\right),\tag{4.2}$$



Figure 4.1: (a) The temporal profile of the combined pulse (blue) represented in a three-dimensional coordinate space of E_x , and E_y ; and its projections to each plane, respectively. (b) The temporal profiles of the right (blue) and the left (red) circular polarization amplitudes. (c) Calculated time-varying polarization ellipticity. (For the definition, see the text.) The arrows in (b) and (c) represent the peak positions of the individual half-cycle pulses.

instead of using semi-major and semi-minor axes. This definition of the polarization ellipticity ε can be further simplified as,

$$\varepsilon(t) = \tan^{-1} \frac{\left|\tilde{E}_L(t)\right|}{\left|\tilde{E}_R(t)\right|} - \frac{\pi}{4},\tag{4.3}$$

so ε is in fact the ratio of the right- and left-circular polarization amplitudes.

To examine the nature of the polarization state change, we consider a polarization shaped THz pulse, given as a sum of two orthogonally polarized half-cycle pulses, as

$$\vec{E}(t) = \hat{x}e^{-(t-t_1)^2/\tau^2} + \hat{y}e^{-(t-t_2)^2/\tau^2},$$
(4.4)

where τ is the gaussian pulse duration, t_1 and t_2 are the time delays of the pulses. For simplicity, $\tau=1$ ps, $t_1=3$ ps, and $t_2=4$ ps are chosen. Figure 4.1 (a) shows the numerical calculation for the temporal profile and the polarization state change of the shaped THz pulse, which shows that the electric field starts being polarized along the *y*-axis, becomes left-circularly polarized, and ends being linearly polarized along the *y*-axis.

The polarization amplitudes $|\tilde{E}_R(t)|$ (blue) and $|\tilde{E}_L(t)|$ (red), are drawn in Fig. 4.1(b), and the polarization ellipticity in Fig. 4.1(c). The results confirm that the polarization state changes sequentially from linear, left-circular, and back to linear polarization states.

4.3 Experimental description

Experiments were performed in a THz time-domain spectroscopy setup. The laser source was a Ti:sapphire laser oscillator which produced 100-fs pulses at a repetition rate of 100 MHz, and the central



Figure 4.2: Experimental setup for the generation of polarization-shaped THz waves. (Inset) Laser beam is refracted from a single glass wedge to the edge of an InAs disk pattern, where the azimuthal angle θ and the thickness l of the glass wedge determine the polarization and timing of the generated THz pulse, respectively. When a set of glass wedges of different azimuthal angles and thicknesses is used at the same time, as-many THz pulses are generated simultaneously from the various locations in the InAs disk and the combined THz wave is made with non-linear polarization.

wavelength was 840 nm. The laser pulses were illuminated on an InAs thin film to generate THz pulses, as shown in Fig. 4.2. For the generation of polarization-shaped THz pulses, a disk-pattern of the InAs film was used. The InAs disk pattern was fabricated similarly to our previous work [88]. The (100)-oriented InAs thin film was grown by molecular beam epitaxy on AlAsSb buffered GaAs substrates. The grown InAs film and the AlAsSb buffer thicknesses were 900 nm and 2200 nm, respectively. Before the substrate was etched, we deposited the metallic hole pattern on the InAs thin film by photolithography and lift-off process for this present work. The diameter of the disk was 200 μ m, and the laser spot of ~5 μ m diameter on its circular edge acted like a THz single point generator at the far-field. For THz detection, a microlens-coupled interdigital photoconductive antenna (PCA) was used [89]. Both the x and y polarization components were measured by rotating the PCA, as the PCA itself is capable of polarization sensitive detection [90].

In order to deliver the laser spots on specific angular locations of the InAs disk edge, we have devised a diffractive optical system made of a set of glass wedges. From a single edge, for example, a collimated laser beam is diverted, as shown in an inset figure of Fig. 4.2, to an angle $\phi = \sin^{-1}(n \sin \alpha) - \alpha$, where *n* is the index of reflection and α is the apex angle of the glass wedge, and focused by a transform lens of focal length f. Then, the laser intensity at the InAs film plane (X, Y) is given by

$$I'(X,Y) = |\int \int \sqrt{I(x,y)} w(x,y) e^{-i\frac{k}{f}(xX+yY)} dxdy|^2,$$
(4.5)

where I(x, y) is the laser intensity at the wedge plane, w(x, y) is the spatal phase modulation induced by the wedge, and k is the propagation constant [50]. The spatial phase modulation w(x, y) is given by

$$w(x,y) = e^{ik\sin\phi(x\cos\theta + y\sin\theta)},\tag{4.6}$$

where θ is the azumuthal angle of the wedge, and Eq. (4.5) becomes

$$I'(X,Y) = \left| \int \int \sqrt{I(x,y)} e^{-i\frac{k}{f} [x(X-X_w) + y(Y-Y_w)]} dx dy \right|^2, \tag{4.7}$$

where $(X_w, Y_w) = (f \sin \phi \cos \theta, f \sin \phi \sin \theta)$. Therefore, the laser beam is focused at (X_w, Y_w) in the InAs flim.

In our experiments, f=12 mm and $\phi=0.5^{\circ}$ were used to satisfy $f \sin \phi = d/2$, where d was the diameter of the InAs disk. Therefore, as a function of the angle θ of the glass wedge, the laser beam was directed to the angular spot $(X, Y) = d/2(\cos \theta, \sin \theta)$ on the edge of the InAs disk. For the laser spot small enough compared to the InAs disk, the photo-Dember current flew generated perpendicularly to the hole edge in the plane, and the emitted THz field E(t) was polarized along the direction of θ , as

$$\vec{E}(t) = \hat{\theta} E_{\text{one}}(t), \tag{4.8}$$

where $\hat{\theta} = \hat{x} \cos \theta + \hat{y} \sin \theta$, and $E_{\text{one}}(t)$ is the electric field time trace of a single THz pulse emitted by a laser spot on the InAs film. As $\hat{\theta}$ was changed from 0°-360° by rotating the glass wedge, an arbitrary direction for a linearly polarized THz field was obtained.

For the generation of a complex polarization state of a THz pulse, multiple glass wedges were used as shown Fig.4.2. We used two sets of multiple glass wedges, 4 and 6, in our experiment. The four different angular positions at $\theta=0^{\circ}$, 90° , 180° , and 270° were illuminated by using a set of four glass wedges, or the six different angular positions among $\theta=0^{\circ}$ - 360° with $\Delta\theta=60^{\circ}$ by six glass wedges. All the glass wedges induced the same diversion angle ϕ , and the beam through each glass wedge was temporally delayed by each additional glass plate of thickness. Note that similar temporal separation techniques have been used elsewhere, for example, the echelon techniques for femtosecond pump probe spectroscopy [91] and single shot THz time domain spectroscopy [92]. In our technique, however, spatial control by glass wedge refraction was included and laser beam was focused to N different spatial locations $(d/2\cos\theta_n, d/2\sin\theta_n)$, for n = 1 - N, with different timing $t_n = (n_w - 1)l_n/c$, where n_w is the refractive index of the glass wedges and c is the speed of light. The resulted THz field is given as a sum $E_{\text{total}}(t)$ that can be written as

$$E_{\text{total}}(t) = \sum_{n=1}^{N} \hat{\theta}_n E_{one}(t-t_n), \qquad (4.9)$$

and, by properly choosing each $\hat{\theta}_n$ and t_n , a number of THz pulses of distinct polarization state were synthesized.

4.4 Results

First, we check the polarization linearity of a simple THz pulse as a function of the azimuthal angle θ of a single glass wedge. Figure 4.3 shows the measured result: the peak amplitudes of the THz pulse



Figure 4.3: Electric filed $\vec{E}(t)$ of a linearly-polarized THz pulse measured by a polarization-sensitive detector as a function of the azimuthal angle θ of a glass wedge: (a) The measured x-polarized component, $\hat{x} \cdot \vec{E}(t)$; (b) The measured y-polarization component, $\hat{y} \cdot \vec{E}(t)$; (c) The the THz peak amplitudes of (b) and (c) plotted as a function of θ , where the dotted lines are $\cos \theta$ (red) and $\sin \theta$ (blue); (d) The polarization angle $\tan^{-1}(\hat{x} \cdot \vec{E}(t)/\hat{y} \cdot \vec{E}(t))$ calculated from (c).

measured along the two orthogonal linear polarization directions, x and y, are plotted as a function of θ , in Figs. 4.3 (a) and 4.3 (b), respectively. Their peak amplitudes show the sinusoidal behaviors of $\cos \theta$ and $\sin \theta$, respectively, as shown in Fig. 4.3 (c), and the calculated polarization angle shows linear to the azimuthal angle θ of the glass wedge, as in Fig.4.3 (d). So, the polarization vector becomes $\hat{\theta} = \hat{x} \cos \theta + \hat{y} \sin \theta$, as expected in Eq. (4.8).

Figure 4.4 shows the result of a four-glass wedge experiment. The four different THz pulses were overlapped in time, with individual linear polarization direction and of individual time delay. So, a non-linear polarized THz wave was generated, as shown in Fig. 4.4 (a). Along the propagation direction, the electric field vector rotated about $\frac{3}{2}\pi$ angle in radian. The thickness and the azimuthal angle of each glass wedge were chosen as $(l_n, \theta_n) = (3 \text{ mm}, 270^\circ)$, $(4 \text{ mm}, 0^\circ)$, $(5 \text{ mm}, 90^\circ)$, and $(6 \text{ mm}, 180^\circ)$, respectively, in serial order as drawn in the inset of Fig. 4.4 (a). With this arrangement of the glass wedges, the delay times and the polarization directions of the individual THz pulses are given as $(t_n, \hat{\theta}_n) = (1.5 \text{ ps}, -\hat{y})$, $(3.0 \text{ ps}, \hat{x})$, $(4.5 \text{ ps}, \hat{y})$, and $(6 \text{ ps}, -\hat{x})$, respectively. The resulting THz wave (blue) is plotted in Fig.4.4 (a), along with the three projections to the *x*-polarization (black) and the *y*-polarization (green), and their parametric (red) planes, where the dots represent the experimental result and the lines the simulation. For the simulation, we have used a numerical fit to the single THz waveform measured in Fig. 4.3, with a function of $E_{\text{one}}(t) = c_1 \exp(-t^2/c_2^2) - c_3 \exp(-(t-c_4)^2/c_5^2)$, where $c_{1,2,\dots,5}$ are fitting parameters. Figure



Figure 4.4: (a) THz pulse shaping with four glass wedges. The inset shows the orientation of the glass wedges. (For the detail, see the text.) Four THz pulses which are linearly polarized are weaved to make circularly polarized THz wave. (b) Calculated right-circular polarization amplitude $|\tilde{E}_R(t)|$ (blue) and left-circular polarization amplitude $|\tilde{E}_L(t)|$ (Red). (c) Calculated polarization elipticity $\varepsilon(t)$. The dots represent the experimental data and the solid line the numerical simulation. The dashed lines along $\varepsilon(t) = \pm \pi/2$ indicate perfect circular polarization.

4.4 (b) shows the amplitude absolute of the left- and right-circular polarization components, $|\tilde{E}_R(t)|$ and $|\tilde{E}_L(t)|$, respectively, as defined in Eq. (4.1). The polarization ellipticity is plotted in Fig. 4.4 (c). The polarization rotation of the generated THz wave is less than 2π , so defining the ellipticity based on the principal axis of Poincaré representation may be inadequate. Instead, we use the ellipticity parameter $\varepsilon(t)$, defined in the Eq. (4.2), to describe the polarization change. The dots in Fig. 4.4 (c) denote the experimental data and the solid line the simulation, which shows that the THz wave began with linear polarization, gradually became non-linearly polarized, and ended back to a wave of linear polarization.

Figure 4.5 shows the result of a six-glass wedge experiment. In this experiment, six glass wedges with thickness of 3, 3.6, 4.2, 4.8, 5.4, and 6 mm, respectively, were used, and their time delays were given as t_n are $t_n = n \times 0.9$ ps for n=1-6. Two types of time-varying polarization states were made, with two sets of glass wedge arrangements, as shown in the insets of Figs. 4.5 (a) and (d), where the direction of the arrows represents the azimuthal angle θ_n and the number in the parentheses represents the thickness ordering n of the glass wedges. In the first example shown in Figs. 4.5 (a)-(c), the azimuthal angles were given as $\theta_n = 270^\circ$, 330° , 30° , 90° , 150° , 210° for n=1 to 6 (from the first to the last). With this arrangement, the polarization unit vectors $\hat{\theta}_n$ were $\hat{\theta}_1 = -\hat{y}$, $\hat{\theta}_2 = \frac{\sqrt{3}}{2}\hat{x} - \frac{1}{2}\hat{y}$, $\hat{\theta}_3 = \frac{\sqrt{3}}{2}\hat{x} + \frac{1}{2}\hat{y}$, $\hat{\theta}_4 = \hat{y}$, $\hat{\theta}_5 = -\frac{\sqrt{3}}{2}\hat{x} + \frac{1}{2}\hat{y}, \hat{\theta}_6 = -\frac{\sqrt{3}}{2}\hat{x} - \frac{1}{2}\hat{y}.$ As a result, the polarization state evolved in time from linear, right circular, and back to linear. The next example is shown in Figs. 4.5 (d)-(f). In this case, the glass wedges werer arranged with $\theta_n = 270^\circ$, 30° , 150° , 210° , 90° , 330° , as shown in the inset of Fig. 4.5 (d), and their thickness was the same as the above case. Then, the polarization direction of the constituent single THz pulses were given as $\hat{\theta}_1 = -\hat{y}, \, \hat{\theta}_2 = \frac{\sqrt{3}}{2}\hat{x} + \frac{1}{2}\hat{y}, \, \hat{\theta}_3 = -\frac{\sqrt{3}}{2}\hat{x} + \frac{1}{2}\hat{y}, \, \hat{\theta}_4 = -\frac{\sqrt{3}}{2}\hat{x} - \frac{1}{2}\hat{y}, \, \hat{\theta}_5 = \hat{y}, \, \hat{\theta}_6 = \frac{\sqrt{3}}{2}\hat{x} - \frac{1}{2}\hat{y}.$ The measured electric field, the calculated amplitude absolutes of the left- and right-circular polarization components, and the polarization ellipticity are shown in Figs. 4.5 (d), (e), and (f), respectively. With this arrangement of glass wedges, the polarization state alternates between the right- and left-circularly polarizations.

4.5 Discussion

Now we discuss the validity of the presented THz polarization shaping technique. The arrangement of N laser pulses on as-many angular positions of the circular edge of a small InAs disk becomes technically valid if the laser spot size becomes significantly smaller than the the radius of the InAs disk pattern. So, the maximum number of wedges is determined by the relation between the size of focused laser spot and the geometrical factors of the glass wedges. Suppose that the glass wedges are of a square shape of length L, which is the maximally allowed size for incoming laser beam. Then, the lateral size d of the laser spot is given by,

$$d = \frac{2f\lambda}{L},\tag{4.10}$$

where λ is the wavelength of the femtosecond laser. In our experimental condition, $d \approx 0.02 \text{ mm}^2/L$. Considering the size of the InAs pattern, that is $D = 200 \mu \text{m}$, and the validity condition, $D \gg d$, we can estimate that the number of allowed angular positions for the focused laser spots, given approximately as A/L^2 , where A is the lens area, reaches up to a few hundreds. Therefore, a few hundreds of glass wedges could be used in the THz pulse shaping method.

It is also worth to discuss about a proper size for the InAs pattern. If the diameter of the pattern D is increased, the experimental condition easily follows the postulation that femtosecond laser spots should be much smaller than the pattern size. However, at the same time, the spatial distribution of the THz emission points gets increased, causing an amplitude loss of the resulting net THz wave. For an estimation, we use Fourier optics theory to estimate this loss η , which is given by

$$\eta = 1 - \frac{2J_1(\pi f_\# D/2\lambda_{THz})}{\pi f_\# D/2\lambda_{THz}}$$
(4.11)

where J_1 is the first-order Bessel function of the first kind, λ_{THz} is the wavelength of the THz wave, and $f_{\#}$ is the *f*-number of its focusing optics. In our experiment, $f_{\#} = 1$, and the amplitude loss ratio is estimated less then 10% for the most part of the frequency range of the generated THz waves. If we used a circular pattern with $D = 600 \ \mu m$, a 30% amplitude loss at 0.5 THz is expected.

4.6 Summary

In summary, we have presented a THz pulse-shaping technique for polarization state control, by superposing a number of THz pulses of various linear polarization vectors. For this, a number of femtosecond optical pulses were arranged spatially and temporally with a set of glass wedges of various thickness, and were used to illuminate on various angular locations of the circular edge of a InAs disk pattern. Then, the lateral photo-Dember currents off from the edge interface generated linearly polarized THz pulses, whose polarization direction was determined by the direction of the currents. For experimental demonstration, we used two systems made of four or six glass wedges to synthesize various unconventional polarization states, such as polarization rotation and alternation between circular polarization states.



Figure 4.5: Examples of THz pulse shaping with six glass wedges. (a-c) THz pulse shaping for polarization rotation: (a) The electric field $\vec{E}(t)$ is plotted in a three-dimensional space defined by E_x , E_y , and time. The dots represent the experimental data while the solid line the simulation. The inset shows the glass wedge arrangement, where the arrows indicate the glass wedge orientation, and the ordering number indicates the glass thickness. (b) Amplitude absolutes of the calculated right- and left-circular polarization components, $|\tilde{E}_R(t)|$ (blue) and $|\tilde{E}_L(t)|$ (red), respectively. (c) Polarization ellipticity $\varepsilon(t)$, which shows that polarization changes from linear, right-circular, and back to linear in one-cycle time duration. The dashed line at $\varepsilon(t) = \pi/2$ ($-\pi/2$) indicates perfect left (right) circular polarization state. (d-f) THz pulse shaping for polarization alternation: (d) Electric field vector, (e) Circular polarization amplitude absolutes, (f) polarization ellipticity. Polarization state changes from right circular to left circular.

Chapter 5. Sub-wavelength diffraction and phase shift anomalies caused by it

In previous chapters, we have described diffraction imaging and polarization shaping techniques with ordinary Fourier optics theory or scalar diffraction theory. In this chapter, we study sub-wavelength diffraction phenomena which can't be explained by scalar diffraction theory.

Terahertz time-domain spectroscopy system has great advantages to study these phenomena. First, with ultra-broad bandwidth THz waves, studying diffraction phenomena with many scale factors, aperture scale over wavelength, is easily possible without many experiment samples. Second, we could also study phase behaviors of sub-wavelength diffraction as well as amplitude behaviors. In addition, subwavelength structures can be easily fabricated for THz experiments, and experiments with real metals can be treated as experiments with ideal perfect conductors due to dielectic properties of real metals in THz range [93].

Research results including both experiments and theories in this chapter are published in Optics Letters Vol. 35 pp. 508-510 (2013), entitled "Phase-shift anomaly caused by sub-wavelength-scale metal slit or aperture diffraction."

5.1 Introduction

Electromagnetic wave diffraction through an aperture, such as a slit or a circular hole, has been fully explained with the Kirchhoff's scalar diffraction theory when the size of the aperture, d, is large compared to the wavelength, λ , of the electromagnetic wave [35, 36]. However, as Bethe pointed out [94], the diffraction phenomena from an aperture is not consistent with this scalar diffraction theory when the size of the aperture becomes equivalent to, or smaller than, the wavelength, and vectorial nature of the electric and magnetic fields needs to be considered.

After Bethe's theoretical expectation, the subject of sub-wavelength aperture transmission has been one of the important research topics under active investigations. Furthermore, the latest emergence of near-field optical applications and sub-wavelength resolution imaging has even fueled the desire to better understand the sub-wavelength diffraction phenomena in various experimental situations [95, 96, 97]. Some of the examples are the sub-wavelength transmitted power, the propagation distribution, local field enhancement, and so on [98, 99, 100, 101, 102, 103, 104, 119, 120, 121, 122]. To list a few, the extraordinary power transmission phenomena in sub-wavelength groove patterned slits [119, 120], more recently, the Fabry-Perot-like behaviors in thick-slit transmission [121, 122] and strong field enhancement in small width slits are experimentally observed and theoretically explained [103, 104].

Recently, phase studies of electromagnetic waves becomes also more important because phase properties of few-cycles or even sub-cycle electromagnetic waves are used in various research areas [105, 106, 107, 108, 109]. In optical frequency, application research such as wave plate design based on phase shift properties [123, 124] of sub-wavelength diffraction are on-going. Since a phase measurement is easily achieved from a time domain signal in terahertz frequency region, some papers studied anomalous phase shift in sub-wavelength near-field transmission with this frequency range experiment [110, 111]. In this chapter, we develop a phenomenological theory for sub-wavelength diffraction problem, and verify its predictions by the direct field measurement of terahertz time-domain diffraction experiment. We study three types of test geometries, a single slit, a circular aperture, and double slits of sub-wavelength scale, and the diffraction behaviors are investigated as a function of their geometrical factors, aperture scale over the wavelength.

We first study the diffraction phenomena from a sub-wavelength-scale metal slit. The resulting amplitude and phase behavior of the diffracted wave and their polarization dependence exhibit substantially different physics that are not explained by scalar diffraction theory. We note that the disagreement between these phenomena and scalar diffraction theory is attributed to the failure of Kirchhoff's assumption, which is that both electric and magnetic fields in aperture are the same as the incident ones. To remove this disagreement, we set theoretical arguments based on the induction of the electric current [103, 104] and effective magnetic dipole radiation [94]. Our theoretical argument predicts that (1) the transmission amplitude does not linearly scale to the slit width but surprisingly maintains a constant or scales quadratically, depending on the polarization of the incident electric field, and that (2) the transmission phase also changes dramatically from the constant Gouy phase advancement, gaining either a positive or negative additional phase shift, depending on the polarization. Experimental verification of the sub-wavelength slit diffraction shows an excellent agreement of such predictions.

We also study the diffraction phenomena from a sub-wavelength-scale metal circual hole. In this geometry, we only focus phase behavior since amplitude behavior of sub-wavelength hole diffraction is quite well studied for a long time [94, 98]. In a small hole limit, dffraction effectively becomes the magnetic dipole radiation [94], so $\pi/2$ more phase shift from Gouy phase happens in far field compared from a large aperture transmission. The phase shift in the intermediate regime is also calculated and compared with experimental results.

Finally, we study the diffraction phenomena of double slits. Because of phase shift anomalies in a sub-wavelength slit transmission, diffraction pattern in Young's double-slit experiment is modulated from the expectation by scalar diffraction theory. In addition, we find these modulation depends on light polarization because phase shift anomalies are strongly related to it.

5.2 General theory of phase shift anomaly in sub-wavelength diffraction

Let us consider a linearly polarized electromagnetic wave of angular frequency ω and wave number $k = \omega/c$ propagating along z-direction diffracts through an aperture located at z = 0. A time varying phase factor $e^{-i\omega t}$ are skipped in following all equations. When the aperture is a perfect conductor and large enough so that the aperture edge effect is ignored, the diffracted wave in the far-field region at $\vec{R} = (X, Y, Z)$ is given according to Kirchhoff's scalar diffraction theory [35] by

$$\vec{E}_T(\vec{R}) = -i\frac{ke^{ikR}}{2\pi R} \int \int_{\Sigma} \vec{E}_0 e^{-ik\frac{xX+yY}{R}} \emptyset dxdy,$$
(5.1)

where E_T represents the diffraction of the transmitted wave, Σ denotes the aperture plane, \emptyset the obliquity factor, E_0 the incident electric field amplitude, $k = \omega/c$, and $R = |\vec{R}|$. The $\pi/2$ phase advance, or $-\pi/2$ phase delay, of $E_T(\vec{R})$ with respect to the e^{ikR} phase factor in plane-wave propagation is caused by the transverse wave confinement through the aperture, and is generally known as Gouy phase shift [112, 113, 114, 115]. We designate this phase shift as ϕ_G .

When a sub-wavelength aperture is used, however, the scalar diffraction theory based on Eq. 5.1 fails because the electric field on the sub-wavelength aperture is not same as the incident electric field and changes as that the shape of the aperture changes. Unlike the electric field, the magnetic field on an aperture does not have such shape dependence due to the symmetric boundary consideration [94] and, therefore, we can classify sub-wavelength diffraction as 2 types: electric field enhanced type and electric field reduced type.

Electric field enhanced type can be understood by induced charges and currents, or plasmon coupling. The induced electric field can be obtained from the vector potential $\vec{A}(\vec{R})$ given by

$$\vec{A}(\vec{R}) = \frac{\mu_0 e^{ikR}}{4\pi_0 R} \int_{\Sigma} \vec{J}(x, y) e^{-ik\frac{xX+yY}{R}} dxdy,$$
(5.2)

where $\vec{J}(x, y)$ is the current density and μ_0 is the magnetic permeability. It is noted that electrostatic potential is ignored in the lowest order perturbation calculation as the net charge accumulation is zero. From electromagnetic theories, equation 5.2 becomes

$$\vec{E}(\vec{R}) = i \frac{kZ e^{ikR}}{4\pi R} \int_{\Sigma} \vec{J}(x,y) e^{-ik\frac{xX+yY}{R}} dxdy$$
(5.3)

where $Z = \sqrt{\frac{\mu_0}{\varepsilon_0}}$. According to Gauss law, a pair of opposite charges are accumulated being in phase with the electric field, so electric current density, $\vec{J}(x, y)$, is induced and its time variance is phase-shifted from the incident electric field as

$$\vec{J}(x,y)/\left|\vec{J}(x,y)\right| = -i\vec{E}_0/\left|\vec{E}_0\right|.$$
 (5.4)

From equations 5.3 and 5.4, we could know the phase of this induced field becomes as

$$\vec{E}_{ind}(R) \propto \vec{E}_0 e^{ikR}.$$
(5.5)

Therefore, this induced field has same phase as the phase factor, e^{ikR} . As a result, diffracted waves from electric field enhanced type apertures have phase retardation compared from normal Gouy phase shift.

Electric field reduced type can be understood by Bethe diffraction [94]. In this type, the electric field is negligibly small, so the diffracted field mainly results from the remain magnetic field. The most convenient way to understand these types of diffraction is Bethe's effective magnetic dipole model [94]. In this model, although they are nonexistent, we could imagine effective magnetic surface density and corresponding magnetic dipole moment satisfying proper boundary conditions of the geometry, and treat diffraction field as this effective magnetic dipole radiation. From the definition of dipole moment, the effective magnetic dipole, \vec{m} , should be

$$\vec{m} \propto -\vec{H}_0. \tag{5.6}$$

where \vec{H}_0 denotes the incident magnetic field. Therefore, the diffracted wave, $\vec{E}_{MD}(R)$, becomes

$$\vec{E}_{\rm MD}(R) \propto -\vec{E}_0 e^{ikR}.$$
(5.7)

As a result, diffracted waves from electric field reduced type apertures have phase advancement compared to normal Gouy phase shift.

5.3 Experimental description

Experimental verification of a sub-wavelength diffraction was performed with transmission-type terahertz (THz) frequency waves. We adopted the waveform capture technique routinely used in a conventional THz time-domain spectroscopy [116, 117] as shown in Fig. 5.1 (a). THz pulses were generated



Figure 5.1: (a) Experimental setup. (b) Knife-edge experiment for THz beam spot and (c) reconstructed THz beam spot sizes. Blue, red, and black lines represent 0.3 THz, 0.4 THz, 0.5 THz, respectively.

from a conventional photoconductive antenna irradiated with femtosecond near-infrared laser pulses from a Ti:sapphire mode-locked laser oscillator [116, 117]. Then the THz pulses were measured via laser-gated electro-optical sampling with a 2-mm-thick $\langle 110 \rangle$ -oriented ZnTe crystal and their time-domain waveforms were recorded as a function of time delay between the THz pulse generation and detection.

Except section 5.6, the diffraction apertures were located at the focus of the THz-TDS in a 8-f geometric configuration composed of four parabolic mirrors or teflon lenses with a f = 100 mm focal length. The plane-wave nature of the THz pulses in the vicinity of the focal area was tested with a knife-edge diffraction experiment as shown in Fig. 5.1 (b) and THz spot is reconstructed in Fig. 5.1 (c). The incident wave could be considered as a plane wave because each spot size of each frequency is about several times larger than the area of the largest aperture. For section 5.6, we will describe experimental geometry in section 5.6.

Apertures were made out of stainless steel, copper, and aluminum with a thickness of 12.8 μ m, 18 μ m, and 18 μ m, respectively. All metals in THz range have very high dielectric constants like perfect conductors [93], so dielectric properties of metals are not considered in this dissertation. Stainless steel apertures are commercial and free standing while copper apertures are on a polytetrafluoroethylene plate with a thickness of 0.8 mm. Aluminum apertures are also free standing and made ourselves by the femtosecond laser micro machining system.

5.4 Sub-wavelength single slit diffraction

First example we consider is the diffraction from a sub-wavelength slit. Our single slit samples were made by 2 methods. First group of single slits were free standing and made out of stainless steel with a thickness of 12.8 μ m, a length of L = 3 mm, and various widths of 30, 40, 50, 100, 150, and 200 μ m, respectively. Second group of single slits were patterned on a 18- μ m-thin copper sheet on a 0.8-mm-thick polytetrafluoroethylene plate with a conventional circuit board manufacturing method without coating. We tested sixteen different sizes of slit width from $d = 100 \ \mu$ m to 700 μ m with a 40- μ m spacing for copper slits.

The slit diffraction problem under consideration is defined as shown in Fig. 5.2, where a linearly polarized electromagnetic wave of angular frequency ω and wave number $k = \omega/c$ propagates along the z-direction and diffracts through a sub-wavelength-scale slit of width $d \leq \lambda$ and length L located at z = 0. We denote the polarization angle of the electric field with respect to the slit orientation by θ and the propagating vector by $R = \sqrt{x^2 + y^2 + z^2}$. The electric field within the slit strongly depends on θ , while the magnetic field does not have such dependence due to the symmetric boundary consideration [94, 35], and, therefore, the physical origin of the resulting transmission wave changes depending on the polarization of the incident field.

5.4.1 Perpendicular polarized electric field

When $\theta = \pi/2$, the waveguide theory predicts the existence of the propagation mode of the electric field, regardless of the size of d [35], and the electric field is even known to be strongly enhanced in small d limit [104, 103]. On the other hand, the magnetic field again remains as much as the incident field, H_0 . Therefore, the transmission wave in this geometry comes from two distinct contributions: The first one is the ordinary diffraction field as expected from the scalar diffraction theory, while the second one is originated from the remained electric field, which is subtraction of the incident electric field from the enhanced electric field.

While the first contribution, denoted as $E_t(R)$, can be calculated from equation 5.1 and is proportional to d/λ , the second contribution, denoted as $E_i(R)$, is quite uncertain. Nevertheless, recent experimental report shows $E_i(R)$ has λ dependence field enhancement compared to the expactation from the scalar diffraction theory [103], so $E_i(R)$ should be a constant of d/λ due to scale invariance, and this phenomenon may be explained by the theory that the induced current flows in a λ -depending distance from the slit edge [104] and k term in Eq. 5.3. Because of the $\pi/2$ phase difference between $E_t(R)$ and $E_i(R)$ due to equation 5.5, the net result of the transmission field amplitude near the optical axis, $E_{\theta=\pi/2}(R)$, is given by

$$E_{\theta=\pi/2}(R) = E_i(R) + E_t(R) = (\alpha + \frac{d}{i\lambda}) \frac{LE_0}{R} e^{i(kR - \omega t)},$$
(5.8)

where α is a proportional constant. Note that, because of the induced field from the slit edge currents, a considerable portion of the incident wave always passes through a sub-wavelength slit in this geometry even in very small d limit [103].

It is noted that the induced electric field contribution, \vec{E}_i , in Eq. 5.8 is $\pi/2$ phase-shifted from the transmitted electric field contribution \vec{E}_t in Eq. 5.8, so the net diffraction electric field have the phase shift anomaly, ϕ_{slit} , as

$$\phi_{\text{slit}} = \tan^{-1} \frac{E_t}{E_i} = \tan^{-1} \frac{d}{\alpha \lambda}.$$
(5.9)



Figure 5.2: Geometry of sub-wavelength single slit diffraction.

It is also noted that the geometrical scaling of \vec{E}_t is given proportional to d compared to \vec{E}_i . As a result, the induced electric field contribution to the diffraction phase becomes gradually significant in the sub-wavelength diffraction regime and, accordingly, the diffraction phase ϕ_{slit} changes from $\pi/2$ (normal Gouy phase shift) to 0 in the limit of extreme sub-wavelength-size slit transmission. In the intermediate regime, both the transmitted and induced fields need to be considered, and the diffraction phase ϕ_{slit} in Eq. 5.9 is given as a function of the ratio of the geometrical factor, $\frac{d}{\lambda}$.

Experimental verification of both amplitude and phase behaviors are performed in transmission type THz-TDS. For the amplitude behavior of sub-wavelength slit diffraction, we use our first slit set, made of stainless steel with a thickness of 12.8 μ m, while we use second slit set, made of 18 μ m copper sheet on a 0.8-mm-thick polytetrafluoroethylene plate, for the phase behavior of sub-wavelength slit diffraction.

The amplitude behavior is shown in Figure 5.3. Fig. 5.3 (a) shows the measurement of the transmitted THz time trace through sub-wavelength-scale slits for $\theta = \pi/2$ case. For studying the relation between transmission and $\frac{d}{\lambda}$ factor, we plot amplitude transmission with the factor in fig. 5.3 (b). To get amplitude transmission, we divide frequency amplitudes of diffracted waves to those of reference waves which are measured without slits. We analyze frequency range between 0.3 THz to 1.3 THz for them. Black lines in fig. 5.3. (b) represents fitting lines based on theoretical expectation in eq. 5.8. There are good agreements between theories and experiments.

Experimental results of the phase behavior are summarized in Fig. 5.4. Optical microscopic image of a typical slit is shown in Fig. 5.4(a) along with the electric and magnetic field directions. In Fig. 5.4(b), the temporal waveforms of the diffracted THz pulses for d = 0.1 mm (blue), 0.3 mm (red), 0.5 mm (green), and 0.7 mm (black) are shown, where the dashed line guides the peaks of the waveforms. As the width of the slit, d, is reduced from the largest to the smallest, the gradual increase of the temporal delay of the peak of the waveform is clearly observed. Figure 5.4 (c) shows the phase shifts extracted for a set of



Figure 5.3: Transmitted THz waves through sub-wavelength-scale slits for $\theta = \pi/2$ case. (a) Measured time signals and (b) their amplitude transmission plotted with d/λ . Black line in (b) represents a fitting line based on eq. 5.8.



Figure 5.4: Measured phase shifts of diffracted THz waves from sub-wavelength-scale slits: (a) Optical microscopic image of a slit and the directions of E and B fields and momentum. (b) Normalized THz waveforms diffracted from slits of d = 100, 300, 500, and 700 μ m (from the top to the bottom). (c) Phase shifts, $\phi_{slit} - \phi_G$, for 0.3, 0.35, 0.4, and 0.45 THz are plotted as a function of d/λ . Black dashed line represents a fitting based on Eq. 5.9. The inset figure in (c) is the log-log plot of $- \tan(\phi_{slit} - \phi_G)$ and d/λ .

selected frequency components (0.3, 0.35, 0.4, and 0.45 THz) from the Fourier-transformed experimental data. All phases are compared from the normal Gouy phases, ϕ_G , which can be measured from a bare polytetrafluoroethylene plate. This result can be understood from Eq. 5.9 The dashed curved line in Fig. 5.4(c) represents the theoretical fitting based on Eq. 5.9. The inset confirms the linear relation of $-\tan(\phi_{\text{slit}} - \phi_G)$ and d/λ satisfied for the sub-wavelength diffraction condition (*i.e.*, $d < \lambda$).

5.4.2 Parallel polarized electric field

When $\theta = 0$, the electric field is negligibly small in this geometry due to the boundary condition on metal, so the diffracted field mainly results from the remain magnetic field. The most convenient way to understand these types of diffraction is Bethe's effective magnetic dipole model [94]. In this model, although they are nonexistent, we could imagine effective magnetic surface density and corresponding magnetic dipole moment satisfying proper boundary conditions of the geometry, and treat diffraction field as this effective magnetic dipole radiation. To be more specific, we calculate diffracted field of this geometry with this model. Here, the effective magnetic surface density should give constant magnetic field, H_0 , inside the slit where H_0 is the incident magnetic field amplitude. For simplicity, we assume that L is long enough that the effective magnetic surface density, $\rho(y)$, has no x-dependence. Then, $\rho(y)$ should be proportional to $-y/\sqrt{d^2/4 - y^2}$ to give uniform magnetic field inside the slit [94]. In addition, the effective magnetic surface density should be proportional to the incident magnetic field amplitude, so it can be written as

$$\rho(y) = -CH_0 \frac{y}{\sqrt{\frac{d^2}{4} - y^2}},\tag{5.10}$$

where C is the proportional constant. We could determine C from electrostatics as following. By Gauss's law,

$$\nabla \cdot H = 4\pi\sigma \tag{5.11}$$

where σ is effective magnetic volume density. Then, the infinitesimal magnetic field dH from Ldy should satisfy $dH2\pi yL = 4\pi\rho(y)Ldy$, so the coefficient, C, also satisfy as the following integral:

$$H_0 = -CH_0 \int_{-\frac{d}{2}}^{\frac{d}{2}} \frac{2y'}{(y-y')\sqrt{\frac{d^2}{4}-{y'}^2}} dy'.$$
 (5.12)

With some calculations, we can get as

$$\int_{-\frac{d}{2}}^{\frac{d}{2}} \frac{y'}{(y-y')\sqrt{\frac{d^2}{4}-{y'}^2}} dy' = -\pi,$$
(5.13)

so we can determine the constant, C, and magnetic surface density, $\rho(y)$, as

$$\rho(y) = -\frac{1}{2\pi} \frac{y}{\sqrt{\frac{d^2}{4} - y^2}} H_0.$$
(5.14)

The effective magnetic dipole moment, m_{eff} , from the magnetic surface density can be calculated as $m_{eff} = \int_{-\frac{d}{2}}^{\frac{d}{2}} L\rho(y)ydy$, so with eq. 5.14, m_{eff} becomes $-H_0d^2L/16$. With this calculated value, the diffracted field near the optical axis, $E_{\theta=0}(R)$, becomes as

$$E_{\theta=0}(R) = -\frac{k^2 d^2 L E_0}{16R} e^{i(kR-\omega t)},$$
(5.15)

where E_0 represents the incident electric field amplitude. The most surprising point of equation 5.15 is that transmission amplitude behavior. The resulting diffracted electric field is proportional to d^2/λ^2 unlike the linear d/λ -dependence expected in scalar diffraction theory or Eq. 5.1. As a result of this scaling discrepancy, the diffracted field from the slit is given much smaller than what is expected from the scalar diffraction theory in the small d limit. We note that similar scale factor difference also exists in sub-wavelength-scale hole diffraction [94]. Another remarkable point of equation 5.15 is phase behavior. Like a discussion in eq. 5.7, phase of diffracted waves are different from normal Goup phase and have 180 degree shifted phase from the phase factor, e^{ikR} .

Experimental verification for $\theta = 0$ case is performed with the set of 6 stainless steel slits in transmission type THz-TDS. Figure 5.5 shows the measurement of the transmitted THz waves through subwavelength-scale slits for $\theta = 0$. For studying the relation between transmission and $\frac{d}{\lambda}$ factor, we also plot amplitude transmission with the factor in fig. 5.5.(b). We again divide frequency amplitudes of diffracted waves to those of reference waves to get amplitude transmission. Black lines in fig. 5.5. (b) represents fitting lines based on theoretical expectation in eq. 5.15. There are good agreements between theories and experiments, and, especially, we note that the relation between amplitude transmission and $\frac{d}{\lambda}$ factor for $\theta = 0$ in fig. 5.5. (b) follows $\frac{d^2}{\lambda^2}$ dependence until just below the cutoff wavelength condition, and the dependence suddenly breaks over the cutoff wavelength condition.

5.4.3 Comparison between $\theta = \pi/2$ and $\theta = 0$

As shown in fig. 5.3 and fig. 5.5, amplitude of diffracted waves for $\theta = \pi/2$ and $\theta = 0$ are totally different. Even in small *d* limit, considerable waves pass through sub-wavelength slit in $\theta = \pi/2$ case. On the other hand, smaller transmission is verified compared to the expectation of the scalar diffraction theory in $\theta = 0$ case. With these results, we will discuss how to make a wire-grid polarizer with high extinction ratio later.

Another remarkable difference between $\theta = \pi/2$ case and $\theta = 0$ case is the phase of diffracted waves. For large slits, phase of diffracted waves in the far field is $\pi/2$ shifted compare to the phase factor, e^{ikR} , and this phenomenon is known as Gouy phase [112, 127, 113, 128, 114]. On the other hand, for very small d, the phase of diffracted electric field is just e^{ikR} or $-e^{ikR}$ in $\theta = \pi/2$ and $\theta = 0$, respectively. For intermediate size slits, the phase shift is between 0 to $\pi/2$ for $\theta = \pi/2$ case and between $\pi/2$ to π for $\theta = 0$ case. These phase shift anomalies are directly measured in our THz waveform detection. Fig. 5.6.(a-f) represent normalized time signals of diffracted THz waves from $30\mu m$, $40\mu m$, $50\mu m$, $100\mu m$, $150\mu m$, and $200\mu m$ slit, respectively. Blue and red lines in fig. 5.6 represent $\theta = 0$ and $\theta = \pi/2$ diffraction respectively while reference signals are plotted in dot lines. Almost $\pi/2$ phase advance and retardation are clearly observed in 30 μm -slit diffraction shown in fig. 5.6. (a). As d, becomes larger, phase difference between $\theta = 0$ and $\theta = \pi/2$ becomes smaller as shown in fig. 5.6. (b-f).

5.4.4 Arbitrary polarizations

Sub-wavelength slit diffraction can be understood as a geometric configuration of $E_{\theta=0}(R)$ and $E_{\theta=\pi/2}(R)$ based on Eqs. 5.8 and 5.15. In our experiment, the THz generation and detection are polarization sensitive [126], the measured field can be expressed as

$$E(\theta, R) = E_{\theta=0}(R)\cos^2\theta + E_{\theta=\pi/2}(R)\sin^2\theta.$$
(5.16)

In experiments, we put a sub-wavelength-size slit on focus point as shown in Fig. 5.1 and measure transmitted THz field with rotating θ . Figure 5.7 summarizes the experimental results. The amplitude spectra of the transmitted THz waves through the tested slits are shown in Figs. 5.7 (a-e), respectively,



Figure 5.5: Transmitted THz waves through sub-wavelength-scale slits for $\theta = 0$ case. (a) Measured time signals and (b) their amplitude transmission plotted with d/λ . Black line in (b) represents a fitting line based on eq. 5.15.



Figure 5.6: Measured electric fields through slits having their width of (a) $d = 30 \ \mu m$, (b) $d = 40 \ \mu m$, (c) $d = 50 \ \mu m$, (d) $d = 100 \ \mu m$, (e) $d = 150 \ \mu m$, and (f) $d = 200 \ \mu m$. All signals are normalized. Red lines represent $\theta = 0$ cases while blue lines represent $\theta = \pi/2$ cases. Dot lines mean reference fields which are measured without slits.



Figure 5.7: The amplitude spectra of transmitted THz pulses from various slits of (a) d=30, (b) 40, (c) 50, (d) 100, (e) 150, and (f) 200 μm , respectively, are plotted as functions of wave direction θ and frequency. (g) Transmission amplitudes retrieved at 0.5 THz depicted with white dashes in (a-e). Dashed lines in (g) represents theoretical expectations in Eq. 5.16. All the amplitudes are normalized by their own maximum transmission amplitudes.

for all polarizations and as a function of frequency, and the amplitude spectra retrieved at 0.5 THz from all slit experiments are compared in Fig. 5.7 (g). Theoretical expectation by Eq. 5.16 is also plotted as dash lines in Fig. 5.7 (g). Theoretical curves and experiments have excellent agreement unless d and λ become comparable. In the small slit limit, Malus law of polarization, or $\sin^2 \theta$ -dependence, is asymptotically satisfied because $E_{\theta=0}(R)$ is much smaller than $E_{\theta=\pi/2}(R)$ in this limit. However, within the experimental range [1/20, 1/3] of d/λ , the $\sin^2 \theta$ -dependence is clearly broken down due to significant $E_{\theta=0}(R)$ in this range. The double minimum points, θ_{\min} , near $\theta = 0$ of the amplitude spectra in Fig. 5.7 (g) are appeared in the condition, $\tan^2 \theta_{\min} = k^2 d^2/16\alpha$, and confirmed by straight forward which explains the induced field effects from the induced current and effective magnetic dipole moment have opposite phase with respect to each other.

5.5 Sub-wavelength circular hole diffraction

In this section, we consider another example, the diffraction from a circular-hole aperture of subwavelength scale. Because transmission amplitude is well studied in this geometry [94, 98], we focus phase shift anomalies of sub-wavelength circular hole diffraction in this section.

With the same experimental procedure of the sub-wavelength slit experiment was taken now with a series of circular-hole apertures. We tested sixteen different sizes of hole radius varied from $a = 100 \ \mu m$ to 475 μ m with a 25 μ m spacing. Those were patterned on a 18- μ m-thin copper sheet on a 0.8-mm-thick polytetrafluoroethylene plate. Experimental results of phase shift anomalies of sub-wavelength circular hole diffraction summarized in Fig. 5.8. We observe that the peak gradually advances for the smaller hole apertures, which direction is opposite to the slit case where the peak was retarded. First of all, the electric fields on a sub-wavelength circular hole apertures are very week compared to incident electric fields unlike electric field enhancement in slit case because tangential part of the electric field on metal is zero and, therefore, sub-wavelength circular hole diffraction is classified in electric field reduced type like sub-wavelength slit diffraction in $\theta = 0$ as we mentioned in Section 5.4.2. On the limit of extreme sub-wavelength-size circular aperture transmission, therefore, it is expected that the diffracted electric field is the radiation from an effective magnetic dipole, \vec{m} , and this effective magnetic dipole and induced field from the dipole should satisfy equations 5.6 and 5.7. Accordingly, the diffraction phase ϕ_d changes from $\pi/2$ (normal Gouy phase shift) to π in the limit of extreme sub-wavelength-size circular aperture transmission. Therefore, the observed phase advancement is consistent with the expectation of $-\pi$ phase shift according to our expectation for the limiting case of the sub-wavelength circular-hole aperture diffraction.

More quantitatively, we can calculate the phase shift of circular-hole diffraction with the help of both Bethe's formal work [94] and the optical theorem [35]: The optical theorem relates the total cross section σ_t to the forward scattering field amplitude, or

$$\sigma_t = \frac{4\pi}{k} Im[f(k=k_0)],$$
(5.17)

where $Im[f(k = k_0)]$ represents the imaginary part of the forward scattering field amplitude. We indicate it as $Im[f(k = k_0)] = E_{Im}/E_0$. In the small aperture limit, $\sigma_t = 128k^4a^6/27\pi$ [94], so E_{Im}/E_0 becomes

$$\frac{E_{\rm Im}}{E_0} = \frac{32}{27\pi^2} \frac{k^5 a^6}{R}.$$
(5.18)

Also, according to Bethe [94],

$$\frac{E_{\rm MD}}{E_0} = \frac{4}{3\pi} \frac{a^3 k^2}{R},\tag{5.19}$$

where $E_{\rm MD}$ denotes the field having $-\pi$ shift from the phase factor as we discussed in section 5.2. Therefore, the phase shift of sub-wavelength diffraction can be obtained as

$$\phi_{\text{hole}} = \phi_{\text{G}} + \tan^{-1} \frac{E_{\text{MD}}}{E_{\text{Im}}} = \phi_{\text{G}} + \tan^{-1} \frac{9\lambda^3}{64\pi^2 a^3},$$
(5.20)

for the small aperture limit $a \ll \lambda$. It is noted that Eq. 5.20 can be also derived in a different approach of the radiation-reaction model from Collin [118]. The dashed line in Fig. 5.8 represents the theoretical expectation in Eq. 5.20 Within the tested range of the hole size, (*i.e.*, $0.1 < a/\lambda < 0.7$), the phase shift changes from 90 degree to zero degree. Since this relation is satisfied in small limit approximation, experimental results and the theoretical expectation are a mismatch. More detailed expectation of the total cross section σ_t [98] may clear this mismatch.



Figure 5.8: Measured data of sub-wavelength circular hole diffraction. Phase shifts, $\phi_{\text{hole}} - \phi_{\text{G}}$, measured at 0.3, 0.35, 0.4, and 0.45 THz are, respectively, plotted with a/λ . Black dashed line represents the theoretical guide line from Eq. 5.20. The inset figure is an optical microscopic image of a typical circular hole.



Figure 5.9: (a) Ordinary Young's double-slit diffraction pattern. (b) Sub-wavelength Young's double-slit diffraction pattern.

5.6 Diffraction pattern modulation in sub-wavelength Young's double-slit experiment

In the previous sections, we discussed sub-wavelength transmission amplitudes and phase from single slits and circular holes. These discussed amplitudes and phases are not expected by scalar diffraction theory, so diffraction patterns from sub-wavelength apertures are also different from scalar diffraction theory. Especially, phase shift anomalies affacts much in diffraction patterns as shown in Fig. 3.1. In this section, we consider sub-wavelength Young's double-slit experiments having different width to show this diffraction pattern modulation.

5.6.1 Theory

Let us consider an aperture of double slits with widthes as d_1 and d_2 is placed z = 0. We assume $d_1 < d_2$ without loss of generality. The distance between slits is a and one slit is placed at x = -a/2 while the other is placed at x = a/2. We assume slit widthes, d_1 and d_2 , are small enough that can be treated as the dirac delta function. Then, a lens with focal length, f, composes Fourier plane as shown in Fig 5.9. Based on scalar diffraction theory, the diffraction amplitude in the Fourier plane is expressed

as

$$E(\omega, x) = \int (d_1 \delta(X + \frac{a}{2}) + d_2 \delta(X - \frac{a}{2})) e^{i\frac{kxX}{f}} dX, \qquad (5.21)$$

where $\delta()$ means the dirac delta function. We ignore constants in equation. 5.21. Then, the diffraction amplitude becomes as $E(\omega, x) = 2d_1 \cos(\frac{ka}{2f}x) + (d_2 - d_1)e^{i\frac{ka}{2f}x}$ and the diffraction pattern, $|E(\omega, x)|^2$, becomes as

$$|E(\omega, x)|^2 = 4d_1d_2\cos^2\left(\frac{ka}{2f}x\right) + (d_2 - d_1)^2.$$
(5.22)

Equation 5.22 represents ordinary Young's double-slit diffraction pattern shown in Fig. 5.9 (a).

If we consider sub-wavelength double slits, then, terms in the integral, $d_1\delta(X + \frac{a}{2}) + d_2\delta(X - \frac{a}{2})$, in Eq. 5.21 fails. Instead of that, we could fix Eq. 5.21 as

$$E(\omega, x) = \int \left(D_1 \delta(X + \frac{a}{2}) e^{\phi_1} + D_2 \delta(X - \frac{a}{2}) e^{\phi_2} \right) e^{i\frac{kxX}{f}} dX,$$
(5.23)

where D_1 and D_2 are transmitted amplitude and not generally same as d_1 and d_2 , respectively, and ϕ_1 and ϕ_2 are phase shift anomalies from Goup phase as discussed in section 5.4. Then, the diffraction amplitude becomes as $E(\omega, x) = D_1 e^{-i\frac{k\alpha x}{2f}} + D_2 e^{i\frac{k\alpha x}{2f} + \Delta\phi}$ where $\Delta\phi = \phi_2 - \phi_1$ and the diffraction pattern, $|E(\omega, x)|^2$, becomes as

$$|E(\omega, x)|^2 = 4D_1 D_2 \cos^2\left(\frac{ka}{2f}x + \frac{\Delta\phi}{2}\right) + (D_2 - D_1)^2.$$
(5.24)

We note 2 things change from Eq. 5.22 to Eq. 5.24. First, the visibility, $V = \frac{I_{\text{max}} - I_{\text{min}}}{I_{\text{max}} + I_{\text{min}}}$ where I_{max} and I_{min} mean the maxium of the intensity and the minimum of the intensity, respectively, changes from $\frac{2d_1d_2}{d_1^2 + d_2^2}$ to $\frac{2D_1D_2}{D_1^2 + D_2^2}$. Second, more surprisingly, diffraction pattern from double slits are shift as much as $\frac{\Delta\phi}{2}$ as shown in Fig. 5.9 (b). Since sub-wavelength transmission amplitudes and phases are strongly related with light polarization, these changes will be different between perpendicular polarization case, which means double slits and polarization of incident THz waves are perpendicular, and parallel polarization case, which means double slits and polarization of incident THz waves are parallel.

5.6.2 Experimental description

To verify this diffraction pattern shift, we set 4-f geometry with teflon lens with f = 100 mm, to define the real plane and the Fourier plane as we did in Section 3.4. Photograph of the experimental setup is shown in Fig. 5.10 with the conceptual drawing of it. To measure diffraction pattern of double slits diffraction, detector scanning may be needed. However, setting movable detection is quite difficult in THz-TDS, so we move both an aperture and lens instead of the movement of the detection part.

Double-slit apertures are free standing and made of a luminum with a thickness of 18 μm . We made them ourselve with 1 kHz Ti:Sapphire amplifier system.

We fabricate 2 double-slit apertures. First sample has widthes with $d_1 = 160 \ \mu\text{m}$, $d_2 = 260 \ \mu\text{m}$, and a distance with $a = 10 \ \text{mm}$. Second aperture has widthes with $d_1 = 1 \ \text{mm}$, $d_2 = 2 \ \text{mm}$, and a distance with $a = 10 \ \text{mm}$. Lengthes of all slits are 100 mm. We denote first and second aperture as aperture 1 and aperture 2, respectively. To change polarization of incident THz waves, we rotate the PCA and ZnTe.

5.6.3 Results

Compare to wavelengthes of THz waves, aperture 1 has sub-wavelength slits while slits on aperture 2 are not sub-wavelength. Therefore, pattern shift based on Eq. 5.24 is only expected on diffraction from aperture 1.



Figure 5.10: Photograph of the experimental setup to measure diffraction pattern of double-slit diffraction. The inset drawing shows the scheme.

Fig. 5.11 shows measured time signals and diffraction patterns at 0.6 THz which are ploted with scanning distance of lens and apertures. Red crosses in Figs. 5.11 (b,f) and blue circles in Figs. 5.11 (d,h) represent experimental data while black dash lines in Figs. 5.11 (b,d,f,h) represent theoretical expectation base on the scalar diffraction theory. Red dash line in Fig. 5.11 (b) and blue dash line in Fig. 5.11 (d) are fitting lines based on Eq. 5.24. All time signals and patterns are normalized.

Measured time signals and diffraction patterns from aperture 1 are shown in Figs. 5.11 (a-d). Measured time signals with perpendicular polarization is ploted in Fig. 5.11 (a) while signals with parallel polarization is ploted in Fig. 5.11 (c). Because transmission waves are far different depending on polarization of the light as discussed in Section 5.4, time signals in (a) and (c) are quite different. Diffraction patterns at 0.6 THz calculated from Figs. 5.11 (a) and (c) are ploted in Figs. 5.11 (b) and (d), respectively. As expected on Section 5.6.1, diffraction pattern is shifted from the expectation of the scalar diffraction theory, and especially, notable pattern shift happens on parallel polarization case.

Measured time signals and diffraction patterns from aperture 2 are shown in Figs. 5.11 (e-h). Measured time signals with perpendicular polarization is ploted in Fig. 5.11 (e) while signals with parallel polarization is ploted in Fig. 5.11 (g). Diffraction patterns at 0.6 THz calculated from Figs. 5.11 (e) and (g) are ploted in Figs. 5.11 (f) and (h), respectively. Because slits on aperture 2 is larger than wavelengthes of THz waves, time signals in Figs. 5.11 (e) and (g) are not much different and diffraction patterns in Figs. 5.11 (f) and (h) well follow the expectation of the scalar diffraction theory.



Figure 5.11: Measured time signals and diffraction patterns from aperture 1 (a-d) and aperture 2 (e-h). All time signals and patterns are normalized. (a,e) Measured time signals with perpendicular polarization. (b,f) Diffraction pattern at 0.6 THz from (a) and (e), respectively. (c,g) Measured time signals with parallel polarization. (d,h) Diffraction pattern at 0.6 THz from (c) and (g), respectively. Red crosses in (b,f) and blue circles in (d,h) represent experimental data. Black dash lines in (b,d,f,h) represent theoretical expectation base on scalar diffraction theory. Red dash line in (b) and blue dash line in (d) are fitting lines based on Eq. 5.24.

5.7 Discussion

5.7.1 Comparison with sub-wavelength Gouy phase shift based on the scalar diffraction theory

It is worth to mention that our previous study on THz wave propagation from sub-wavelength emitters also dealt with the aperture-size dependence of the Gouy phase shift in the sub-wavelength diffraction regime, in which the observed temporal phase shift was explained by the sub-wavelength spatial confinement of the propagation wave [109]. However, the experimental condition for the sub-wavelength emitters, which were the transient Dember dipolar field forced on a 45-degree-tilted semiconductor film is not generalized for the conventional sub-wavelength diffraction problem considered in this dissertation.

5.7.2 A wire-grid polarizer with high extinction ratio

With our study of sub-wavelength slit transmission in section.5.4, we might discuss how to make a wire-grid polarizer with high extinction ratio, defined as $ER = E_{\theta=0}(R)/E_{\theta=\pi/2}(R)$. We consider a wire-grid polarizer as a multi-sub-wavelength slit having width, d, with sub-wavelength spacing, Λ , and fill factor, F, as $F = \frac{d}{\Lambda}$. When the electric field is perpendicular to the slits, or $\theta = \pi/2$, and if $d, \Lambda \ll \lambda$, almost all waves are transmitted whether F is small or large because the contribution from $E_i(R)$ in section 5.4.1 may replenish weakened $E_t(R)$ in section 5.4.1 for small F polarizers. More rigorous theoretical discussion might be found in the reference [129]. Therefore, high extinction ratio is determined by the amount of transmission in $\theta = 0$. When the electric field is parallel to the slits, on the other hand, transmission wave can be understood as the sum of the effective magnetic dipole radiation in eq. 5.15. Therefore, in intuitional point, transmission waves, $E_{\theta=0}(R)$, are expressed as

$$ER \sim E_{\theta=0}(R) \sim \frac{d^2}{\Lambda} = dF = F^2 \Lambda,$$
(5.25)

so wire-grid polarizers with smaller F, Λ , and d have higher extinction ratio. Although we don't consider group effects of slits, our intuitive view is consistent with various experimental reports of THz wire-grid polarizer [130, 131, 132].

5.8 Summary

In this chapter, we have experimentally and theoretically considered sub-wavelength-size aperture diffraction which is not understood by scalar diffraction, and, especially, we focus to study phase shift behaviors. The physical reason of the failure of the scalar diffraction theory in sub-wavelength diffraction is that the electric field on the sub-wavelength aperture is not same as the incident electric field. Instead of that, the electric field can be enhanced or reduced depending on the aperture geometry. As a result, phase retardation from the Gouy phase are appead in E-field enhancing structures and phase advancement from the Gouy phase are appead in E-field reducing structures. Schemetical drawing of these phase shift anomalies is shown in Fig. 5.12, and a brief comparison between sub-wavelength-size slit and circular aperture diffraction and large aperture diffraction based on our study and Bethe's study [94] is shown in Table. 5.1.

For experimental study, we use the direct field capture technique with terahertz time dopmain spectroscopy. With this technique, phase shift behaviors of sub-wavelength transmission is studied as well as amplitude study.
Table 5.1: Summary of amplitude and phase behavior of sub-wavelength-scale diffraction

Charactor	Small Slit($\perp E_0$)	Small Slit($ E_0\rangle$)	Small Circular Hole	Large aperture
Amplitude	no dependence	d^2/λ^2	a^3/λ^2 [94]	(Aperture Area)/ λ
Phase shift	0	π	π	$\pi/2$ or Gouy Phase

We have considered three different geometries. First, we have considered sub-wavelength slit diffraction for both amplitude and phase shift behaviors. Diffraction phenomenon from a sub-wavelength-scale slit is substantially different from that from an ordinary slit, so we apply induced current model for slits perpendicular to the electric field and magnetic dipole model for slits parallel to the electric field. Theoretical argument based on these models in the vicinity of the slit predicts transmission amplitude and phase. From our results, the transmission amplitude does not linearly scale to the slit width but maintains a constant or scales quadratically, and the transmission phase also changes dramatically from the constant Goup phase advancement. Superposition of perpendicular and parallel cases can be applied for arbitrary angle direction slit. Theoretical analyses are in good agreement with the experimental results.

Second, we have considered sub-wavelength circular hole diffraction for its phase shift behavior. For sub-wavelength circular hole diffraction, physical origin of phase shift anomalies is attributed to the magnetic dipole radiation as parallel type slits, so additional phase shifts from the constant Gouy phase advancement are appeared. In addition, we found the phase shift behavior as $\tan(\phi_{\text{hole}} - \phi_{\text{G}}) = 9\lambda^3/64\pi^2 a^3$ in the small hole limit.

Finally, we have considered diffraction pattern in sub-wavelength Young's double-slit experiment. \cos^2 -like diffraction pattern from double slits is symmetric to the optical axis according to scalar diffraction theory. However, phase shift anomalies of sub-wavelength diffraction affacts in diffraction patterns, so \cos^2 -like pattern is shifted in sub-wavelength Young's double-slit experiment. In addition, phase shift anomalies are related to the incident light polarization, these changes also depend on the light polarization.



Figure 5.12: Summary of phase shift anomalies in sub-wavelength-scale diffraction

Chapter 6. Conclusion

Terahertz technologies had been undeveloped for a long time, but they are actively used in many research areas nowadays. One of the core THz technologies is terahertz time domain spectroscopy based on femtosecond laser systems. T-ray in THz-TDS has 2 great advantages compared to T-ray in other THz technologies or other optical sources. First, it has ultra-broad bandwidth or, in other words, it has the frequency-to-bandwidth ratio of near unity. Second, phase measurement by direct field detection with optical gating is convenient. With these unique properties, researches to expand optical physics and applications are in progress.

In this dissertation, we study Fourier optical phenomena using ultra broadband terahertz waves and developed Fourier optical applications such as diffraction imaging and pulse shaping. We also study sub-wavelength diffraction and phase shift anomalies of it. Firstly, we learn that radial information of diffracted pattern can be achieved by spectral analysis of ultra broadband waves, so we propose three different diffraction imaging systems which reduce sampling number drastically. In these three systems, a single pixel detector is only needed to get two dimensional image information. At first, we demonstrate that complex images are reconstructed by only 30 waveform measurements in the coherent optical computer geometry with a hole mask. We also demonstrate even one waveform diffraction imaging is possible with the time separating hole mask. We demonstrate similar scheme with a slanted phase retarder in much higher signal to noise ratio. Our proposed imaging systems can instantly be applied in many THz imaging system for security search or biomedical imaging.

Secondly, we produce polarization shaped few-cycle THz pulse by the illumination of the spatiotemporal controlled femtosecond laser pulses on the circularly metal patterned InAs surface. A set of wedges with various orientations and thicknesses are arranged to get proper spatiotemporal controlling in this technique. As a result, we successfully generate THz waves of various unconventional polarization states, such as polarization rotation and alternation between circular polarization states. Since these kinds of polarizations are very uncommon in traditional optics, we also propose time domain representation of polarization. This polarization shaping technique might be used for spectroscopic studies of circular dichroism in chiral molecules or THz coherent control related with spiral spin state. Because polarization can bring more information, it can also be used in THz communication.

Finally, we study sub-wavelength diffraction and, especially, phase shift anomalies caused by it. It is generally known that $-\pi/2$ phase shift from the propagating phase is exist in usual diffraction and this phase shift is called as the Gouy phase shift. With direct phase measurement in terahertz time domain spectroscopy, we demonstrate that shifting phase can be between 0 to $-\pi$ in sub-wavelength diffraction instead of Gouy phase shift. With comparing Gouy phase shift, nearly $\pi/2$ phase retardation is observed in transmitted waves from a sub-wavelength slit which is perpendicular to the electric field. On the other hand, $\pi/2$ phase advance is observed in transmitted waves from a sub-wavelength slit which is parallel to the electric field or a sub-wavelength circular aperture. We propose the physical origin of these phase shift anomalies as plasmon coupling or magnetic dipole radiation, and theories are in good agreement with the experimental results. From these phase shift anomalies, diffraction patterns are also modulated, and we verify this in sub-wavelength Young's double-slit experiment. For future work, it will be worth checking that diffraction from other sub-wavelength structures follow our physical models. Based on our research results, plasmonic devices such as phase retarders or plasmonic lens could also be developed.

Various other researches with ultra broadband terahertz waves could also be possible. One example is THz-version spectral encoding imaging with ultra broadband terahertz waves instead of a broadband visible light source [133, 134]. The principle of this imaging system is similar to our single-pixel imaging systems in Chapter. 3 except that time frequencies encode real space information instead of spatial frequency information. Developing THz diffractive optics, such as a grating or a prism, is a challenge for it, but plasmonic devices [135] can be used to overcome it.

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Summary

Fourier optical phenomena and applications using ultra broadband terahertz waves

초고속 레이저를 통한 펄스 형태의 테라헤르츠 파 기술은 다른 전자기파 대역에 대비하여 2가지 커다란 장점을 갖는데 이는 초광대역 주파수를 갖는 다는 것과 시간 도메인 상에 전기장을 직접 측정하 여 위상 정보를 얻기가 용이하다는 것이다. 본 논문에서는 이러한 2가지 성질을 이용하여 퓨리에 광학 현상을 관측하고 이를 응용하는 연구를 수행하였다.

본 논문 3장에서는 테라헤르츠 파의 초광대역 주파수를 이용하여 2차원 이미지 정보를 오직 1차원 적인 정보 수집 방식으로 얻을 수 있는 회절 이미징 기술을 개발하였으며 이를 실험으로 입증하였다. 본 논문은 이미지 정보 수집을 각기 3가지 다른 실험에서 수행하였는데 모든 실험들은 측정기가 움직이지 않는 단일 픽셀(single pixel) 측정 방식을 사용한다. 첫번째 실험은 결맞음 광학 컴퓨터(coherent optical computer)을 이용한 것으로 수십 개의 데이터 샘플링만으로도 수백개의 픽셀을 갖는 2차원 이미지가 잘 복원이 됨을 보였다. 두번째 실험은 이러한 결맞음 광학 컴퓨터를 더욱 발전시킨것으로 시간상으 로 테라헤르츠 파를 나누는 마스크를 이용하여 오직 1개의 파형 샘플링으로 2차원 이미지가 복원됨을 보인다. 마지막 실험은 결맞음 광학 컴퓨터 대신 쐐기 프리즘을 이용한 방식으로 결맞음 광학 컴퓨터 방식보다 훨씬 좋은 신호 대 잡음비를 갖는다.

본 논문 4장에서는 초광대역 테라헤르츠 파의 편광을 제어하여 1주기 내에서 편광이 급속도로 바뀌는 새로운 형태의 편광상태를 재단하였다. 이는 원형으로 금속 패턴된 인듐비소 박막에 시공간상으로 재단된 초고속 레이저 빛을 순차적으로 가함으로써 이루어졌는데 본 논문에서는 이를 위해 쐐기 프리 즘이 조합된 새로운 형태의 퓨리에 광학 기기를 개발하였다. 또한 본 논문에서는 재단한 편광 상태를 분석하기 위해 시간 도메인 상에서의 편광 표현 방식을 새롭게 정의하였다.

본 논문 5장에서는 파장이하 회절시 일어나는 여러 현상을 공부하였으며 특히 이때 일어나는 위상 변화를 테라헤르츠 시분해 분광기법을 통한 위상측정을 이용해 측정 및 분석 하였다. 기존의 스칼라 회절 이론에 따르면 회절시 일어나는 위상 변화는 전자기파가 이동하는 거리 대비 -90도이어야 하며 이는 구이(Gouy) 위상 변화로 알려져 있다. 그러나 파장이하 회절에서는 이 위상 변화가 -180도에서 0도까지 일어남을 관측하였는데 이는 회절시키는 aperture상의 경계조건을 만족시키기 위한 전하와 전류 분포 때문이다. 본 논문의 이론에 따르면 전기파가 aperture상에서 강하게 집속되는 경우는 이 동거리 대비 0도의 위상 변화를 보이며 전기파가 aperture상에서 약해지는 경우는 이동거리 대비 -180 도의 위상 변화를 보인다. 이러한 예로써 파장이하 크기의 슬릿 구조와 원형 구멍 구조를 공부하였으며 실험 및 이론이 잘 일치 함을 보였다. 이러한 위상 변화는 회절 패턴에도 영향을 주게 되는데 이에 대한 예로서 본 논문은 영의 더블 슬릿 실험(Young's double-slit experiment)에서 일어나는 패턴의 이동 또한 공부하였다.

감사의 글

이 논문을 완성하기까지 주위의 모든 분들로부터 수많은 도움을 받았습니다. 먼저 학위과정 동안 저를 지도해주신 안재욱 교수님께 진심으로 감사드립니다. 논문 지도뿐 아니라 조언과 충고를 통해 많 은 것을 배울 수 있었습니다. 또한 바쁘신 일정에도 논문 심사를 해주신 김병윤 교수님, 박용근 교수님, 민범기 교수님, 조영달 교수님께 감사드립니다.

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